

# Determination of the longitudinal compressive strength of a Carbon/Epoxy UD ply with bending, compressive and tensile tests

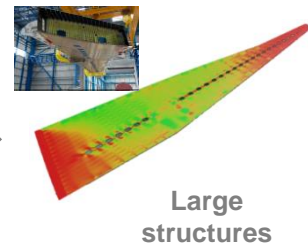
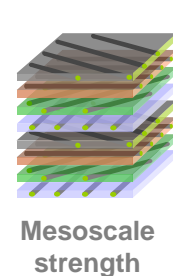
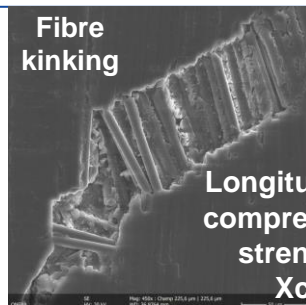
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# Introduction

**$X_c$  is critical for design of large parts**

**Different tests to characterize  $X_c$ :**

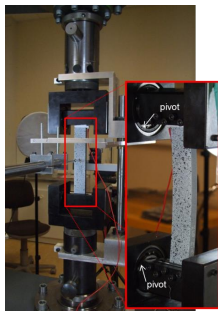
- Are the experimental data consistent ?
- Choice of the modelling scale ?



## Bending tests

**Alternative tests**

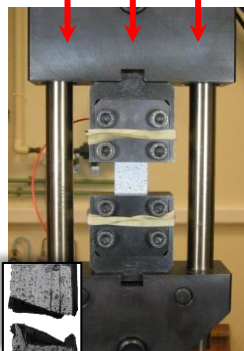
- 4-point bending test
- Compression with pivot device test
- Analysis with FE non linear models
- High strength value



## Compression tests

**Standard tests**

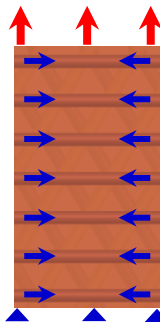
- Load introduction:
  - ASTM D695-15
  - ASTM D3410
  - ASTM D6641
- Compressive tests on UD plies or laminates



## Innovative tensile test

**Innovative tests**

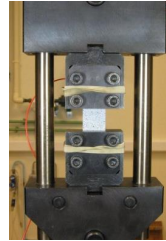
- Optimization of lay-up to fail central 90-ply in longi. compression without any damage
- Tensile tests on a specific laminate



# Compressive tests on UD plies

## Standard compression tests

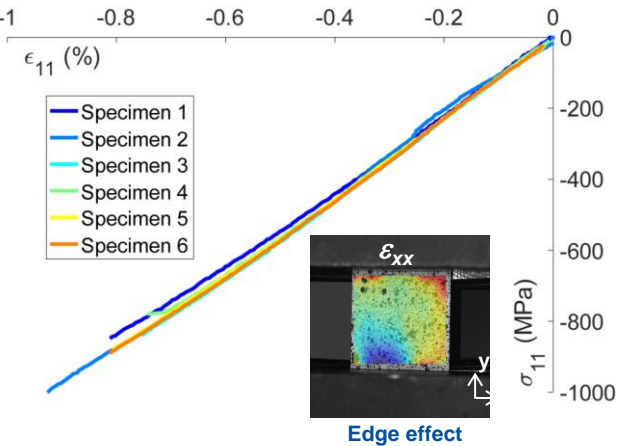
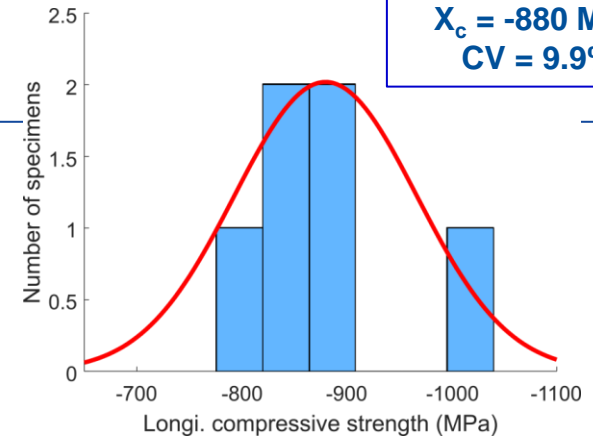
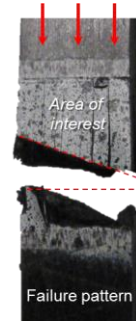
- T700GC/M21 material (268g/m<sup>2</sup>)**  
6 specimens 16 plies - [0<sub>8</sub>]<sub>s</sub>  
manufactured with heating-press at Onera



- Specimens with small free lengths**  
10mmx10mmx4.2mm  
Loading introduced by pushing on edges

[DIN-EN-2850 97]

- Failure pattern analysis:**  
Premature kinking within the tab region [Welsh 96]  
Failure close to the jaws (angle at 15°) [Vogler 01]  
Large scattering (10%) on strength



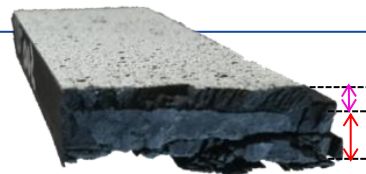
# Bending tests on UD plies

## Bending tests

[Callus 07, Laurin 16]

- Failure mode relevant (no buckling, far from jaws)
- Test analysis with complex FE simulations  
Geometrical and material non linearities (with  $E_{11}^t \neq E_{11}^c$ )
- Very high compressive strengths (from FE simulation)

16 plies



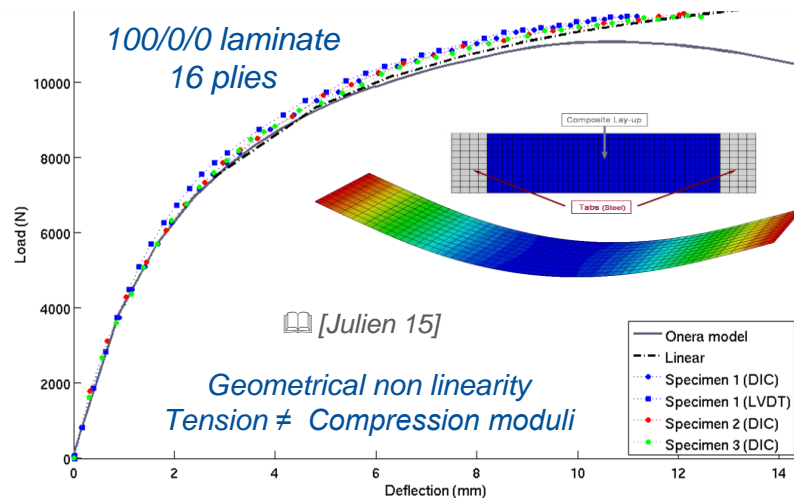
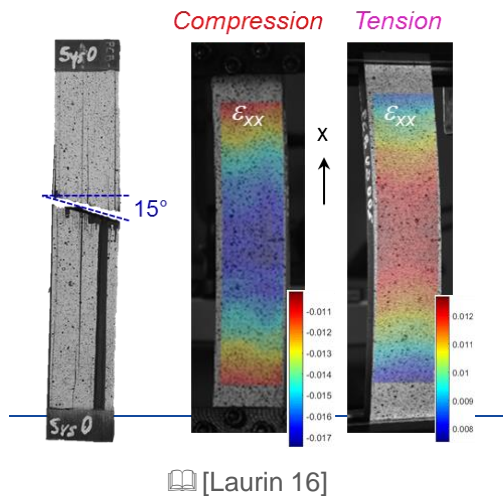
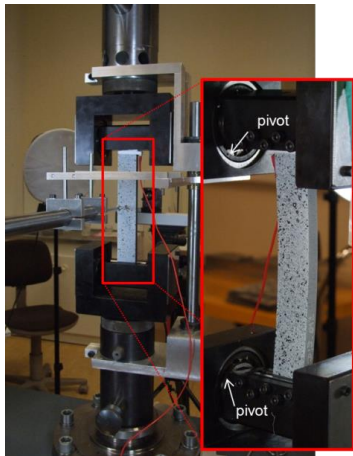
$X_c = -1350 \text{ MPa}$   
CV = 4.5%

32 plies



$X_c = -1220 \text{ MPa}$   
CV = 2.8%

## Compression with pivot



# Innovative tensile tests on a specific laminate

$X_{\epsilon_c} = -1025\text{MPa}$   
 $CV = 1.9\%$

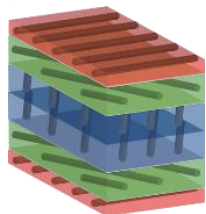
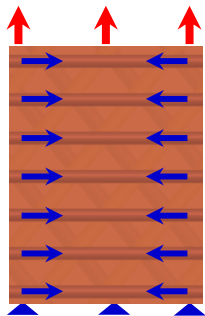
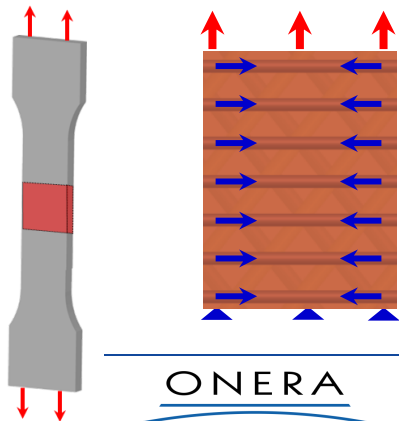
## Proposition of innovative tests

### Tensile test which fails in compression

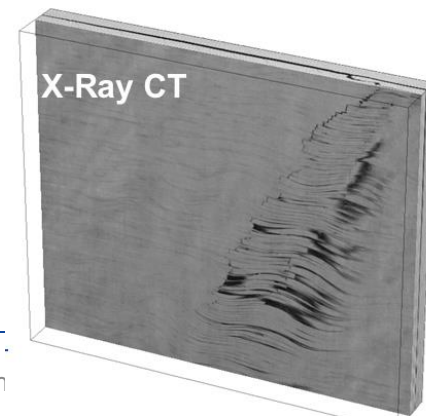
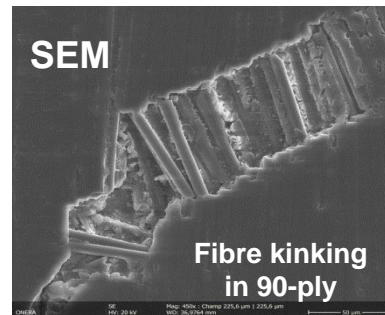
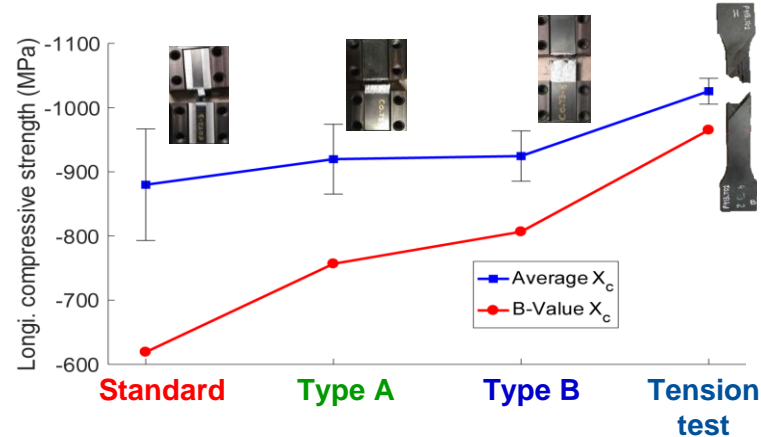
- Tension test on a specific laminate failed by fibre kinking
- Failure is due to **Poisson effect** located at mid-width
- Analysis with CLT extended to non-linear behaviour
- No transverse crack prior failure in compression

### High compressive strengths with low scattering

Value embedded between compression and bending on UD plies



Tensile test  
on specific laminate  
[-30/-45/-30/0<sub>2</sub>/30<sub>2</sub>/45/90<sub>1/2</sub>]<sub>s</sub>



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Determination of the longitudinal compressive strength

# Analysis of the available tensile tests

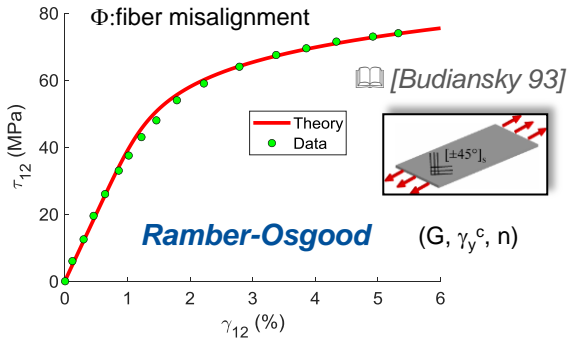
## Model proposed by Grandier *et al.*

### Analytical formula for longi. compression strength $\sigma_c$

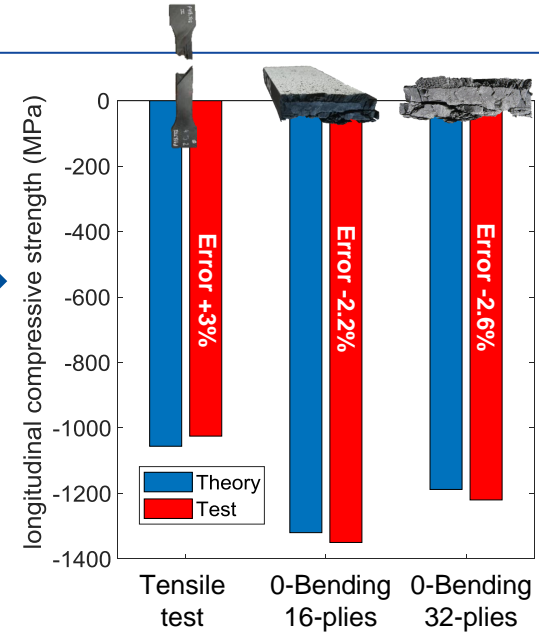
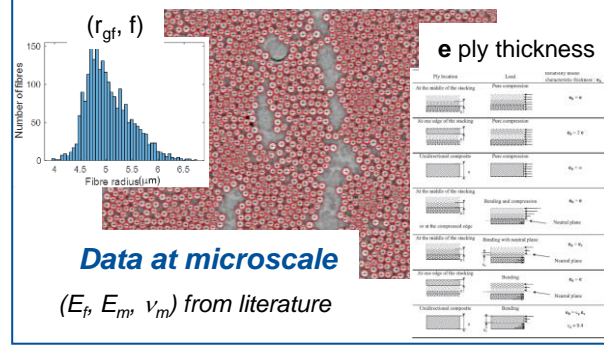
- Based on FE simulations at microscale [Drapier 99], [Gardin 02]
- Take into account type of loadings, ply position, ply thickness

$$\sigma_c = \frac{G}{1 + n \left(\frac{3}{7}\right)^{1/n} \left(\frac{\bar{\phi}/\gamma_y^c}{n-1}\right)^{(n-1)/n}} + (2r_{gf}) \frac{\pi}{e} \sqrt{\frac{E_M E_F}{(1 - \nu_M^2)} f(1-f)}$$

### Micro-buckling mechanism



### Structural effect



Microscale is promising

Test data are consistent (except standard test)



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