

INTERACTIONS BETWEEN DAMAGE EVENTS AND BIOINSPIRED VASCULATURES EMBEDDED IN FIBRE REINFORCED COMPOSITES

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ABSTRACT

The susceptibility of fibre reinforced polymer (FRP) laminate structures to impact damage is well documented. This damage can manifest itself in such a way that significant reductions in mechanical performance result whilst leaving little visual evidence of the impact event (a situation termed *barely visible impact damage* BVID). Microvascular networks that can potentially deliver large volumes of healing resin from an external reservoir to regions of internal damage have been recognised as a means of imparting a self-healing functionality to load bearing FRP structures. Interactions of such vasculature with propagating cracks and damage events is a necessity to ensure release of the contained healing resin, and as such is the subject of this investigation [1].

Unidirectional glass fibre reinforced epoxy (HexPly 913, Hexcel Composites) was selected due to its translucency, allowing easy monitoring of an internal crack front. Steel wire with a diameter of 0.5mm, pre-coated with a PTFE release spray to ease removal post-cure, was selected as the vasculature preform material. For fabrication route A, the vasculature preform wires were located at the laminate mid-plane between the two central plies. To incorporate the steel wires via fabrication route B, the four central plies were cut at the desired vasculature location. Four plies were cut to create the recess necessary for 0.5mm wires based on the nominal ply thickness of the pre-impregnated tape (0.135mm, determined experimentally). The same techniques were used to prepare specimens containing vasculature orientated parallel or transverse to the fibre orientation. Typical micrographs of the resultant vasculature morphologies are provided in Figure 1. Embedding a vasculature transverse to the fibre orientation, via fabrication route A, led to significant fibre waviness and the formation of large resin pockets. The corresponding vasculature formed via fabrication route B shows the elimination of fibre waviness but resin pockets still persist at the corners of the square recess created during fabrication. Alignment of the vasculature to the fibre direction eliminates fibre waviness and resin pockets as the fibres 'fit' around the wire during the laminate cure cycle. The effects of the different vasculature microstructures on the Mode I (Double Cantilever Beam, DCB) and II (End Loaded Split, ELS) interlaminar fracture toughness were evaluated.

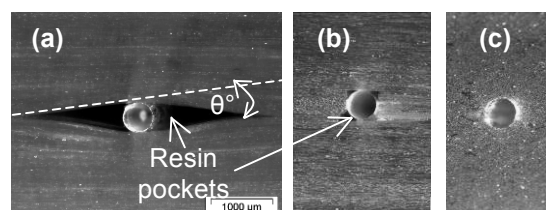


Figure 1: Vasculature characterisation; (a) transverse fabrication route A, (b) transverse fabrication route B and (c) aligned vasculature representative of both fabrication routes.

Vasculature aligned parallel to the fibre and crack propagation direction were cleaved open regardless of fabrication route or opening mode and had little effect on the innate fracture toughness of the host laminate, Figure 2. However, transversely orientated vasculature had significantly differing crack interactions:

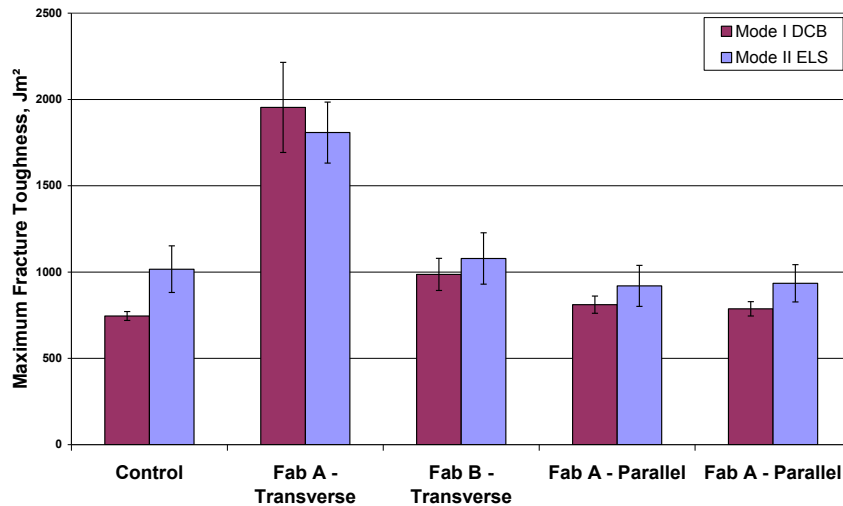


Figure 2: Modes I & II fracture toughness

Fabrication route A – Under mode I opening conditions these vasculae were found to arrest cracks for significant periods leading to exceptional values of fracture toughness at the vasculae locations. However, the build up of strain energy lead to rapid unzipping of the laminate fracture plane on propagation of the crack from the vasculae backface. Under Mode II conditions the crack was arrested at the tip of the resin pocket, then jumped a layer of fibres leading to rapid unzipping of the specimen. This crack propagation path followed the fibre waviness around the vasculae in such a way as resin release would not be expected (Fig 3(b)), and is in agreement with the damage layout formed around a vasculae embedded within a quasi-isotropic carbon fibre laminate [2] using the same fabrication technique (Fig. 3(c)).

Fabrication route B – Cracks were found to breach the vasculae under both Mode I & II conditions (Fig. 3(d) & (e)), leading to moderate crack arrest. Here, the stress concentrations expected at the corner resin pockets caused the vasculae boundary to fail at lower strain energies. The energy stored due to crack arrest at each vasculae was insufficient to cause rapid ‘unzipping’ of the specimens, with the crack being arrested at each subsequent vasculae (if it jumped that far). The opening of the vasculae is a pre-requisite for self-healing, as was confirmed under impact loading (Fig. 3(f)).

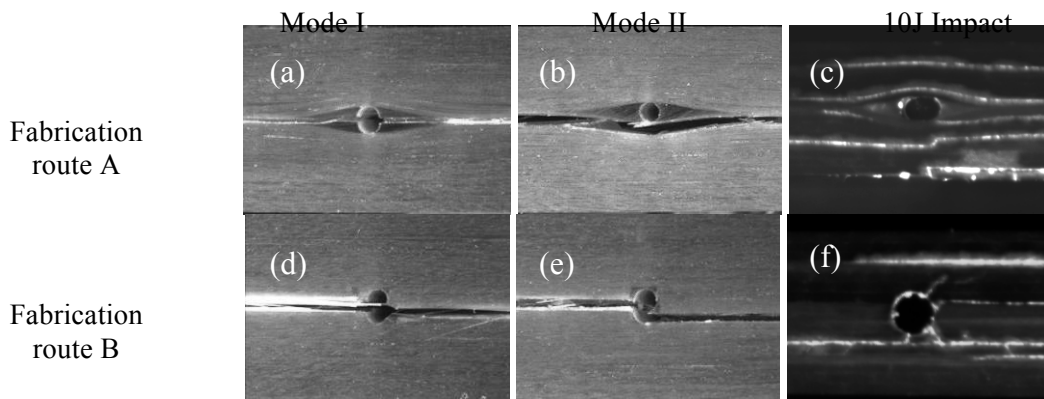


Figure 3: Vasculae-damage interactions

REFERENCES

- [1] Norris, CJ. Bond, IP and Trask RS, Interactions between propagating cracks and bioinspired self-healing vasculae embedded in glass fibre reinforced composites”. *Compos Sci Technol.*, **71**, 2011, pp. 847-853.
- [2] Norris, CJ. Bond, IP and Trask RS, The role of embedded bioinspired vasculature on damage formation in self-healing carbon fibre composites, *Composites A*, **42**, 2011, pp. 639-648.