

Measurement of Fracture Energy for Kink-Band Growth in Sandwich Specimens

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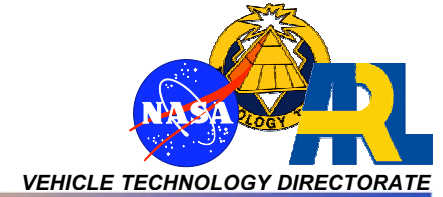
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Mechanics and Durability Branch
NASA Langley Research Center***

CompTest2004, 21-23 September, University of Bristol, UK



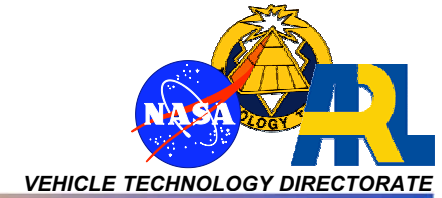
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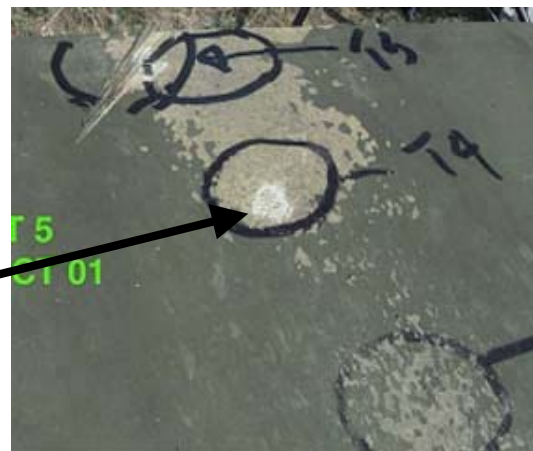
MOTIVATION



Extensive use of sandwich construction in military helicopters



Possible damage
from out-of-plane
loading

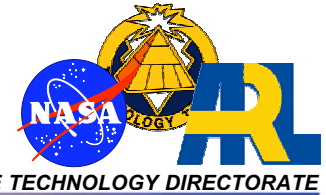


Method needed to
predict compression
after impact strength

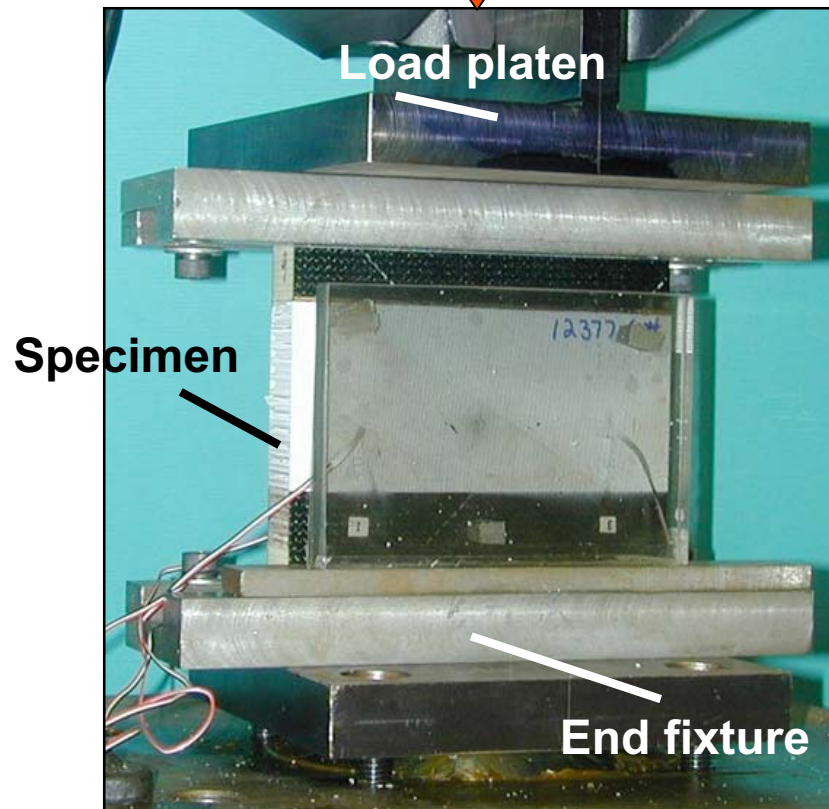


BACKGROUND - CONTINUED

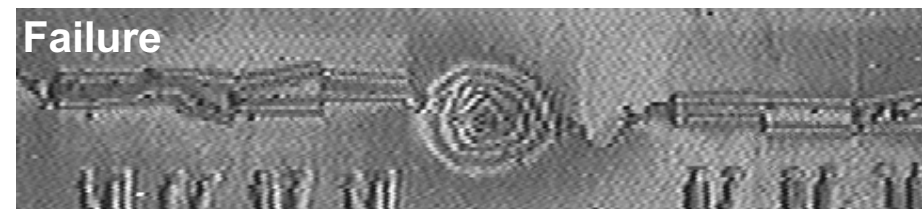
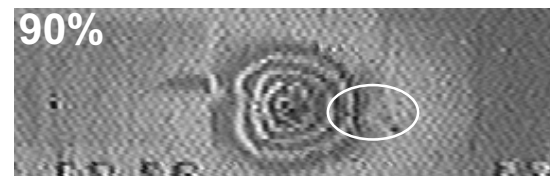
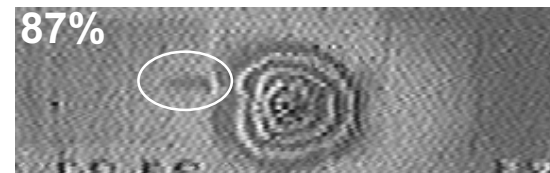
CAI Testing



Specimen loaded under
axial compression



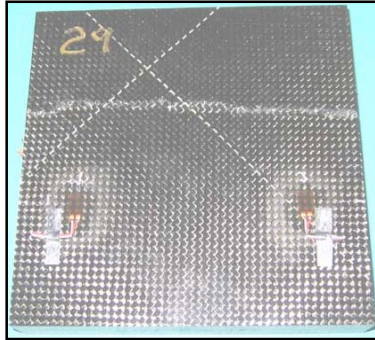
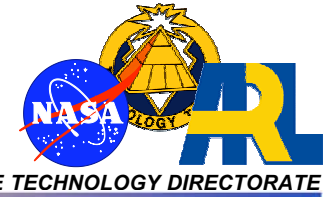
Shadow Moiré Images



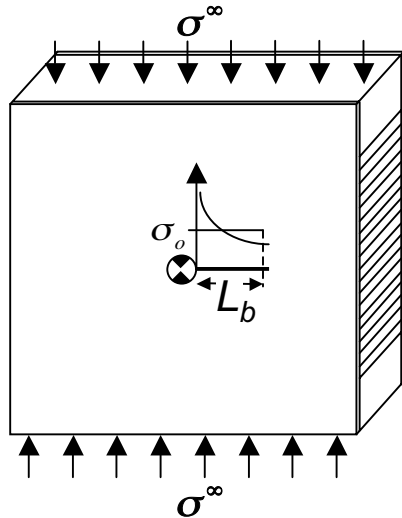


BACKGROUND - CONTINUED

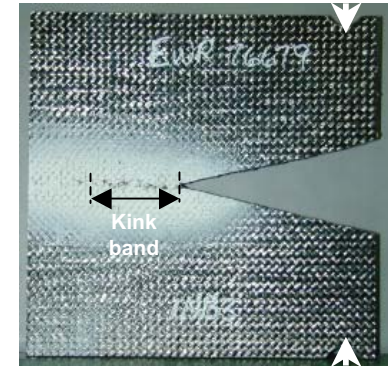
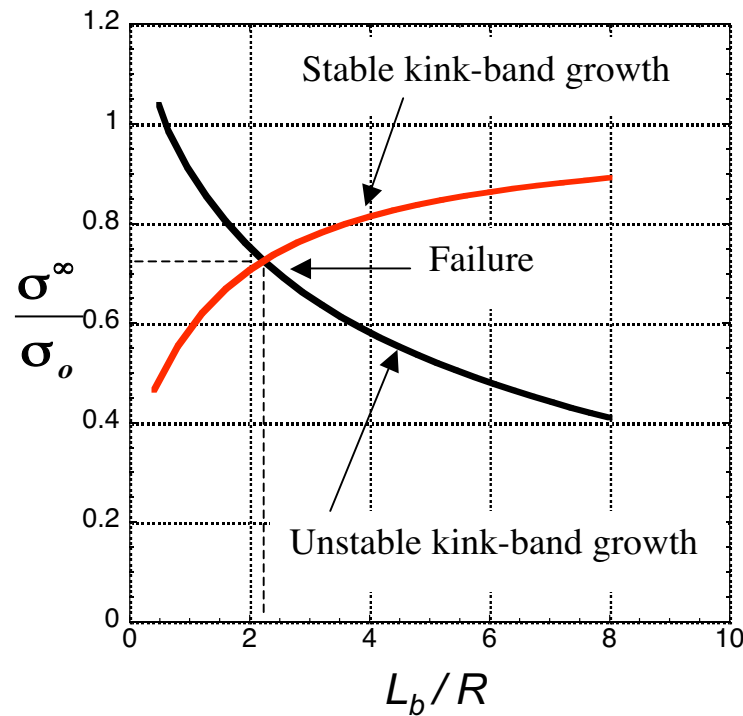
CAI Strength Prediction



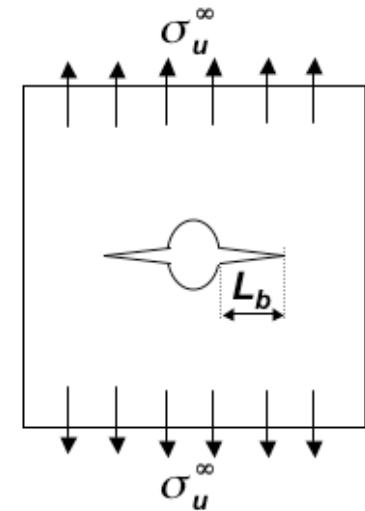
Unnotched strength, σ_o ,
compression test



Average stress criterion used to
calculate stable kink-band growth



K_{Ic} measured from
new fracture test



$$\sigma_u^\infty = \frac{K_{Ic}}{\sqrt{\pi L_b f(L_b / R)}}$$

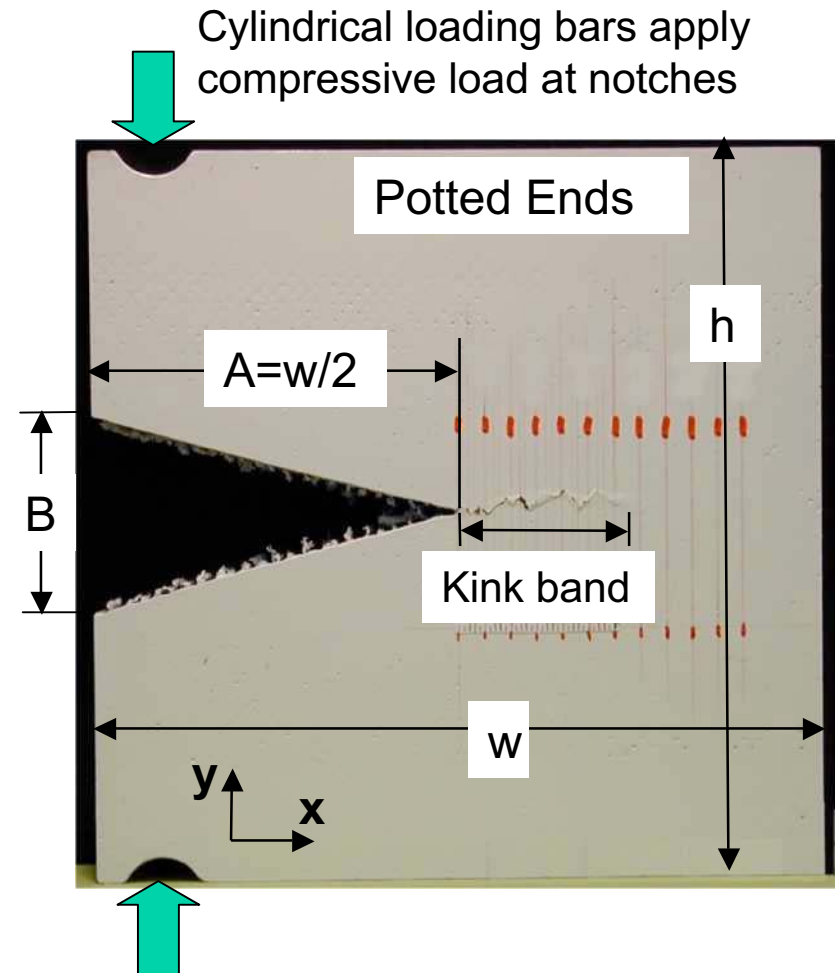


“Compact Compression” Test



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- Test required to measure energy associated with kink-band growth (K_{Ic} calculated)
- Based on compact tension specimen used for metal fracture
- Displacement control (0.5 mm/min)
- Specimen loaded until kink band has extended 5-10mm then unloaded. Process repeated until kink band length is 50mm.
- Dissipated energy calculated for each load cycle
- Critical strain energy release rate, G_{Ic} , calculated for each growth increment
- K_{Ic} calculated from relationship with G_{Ic} for an orthotropic plate





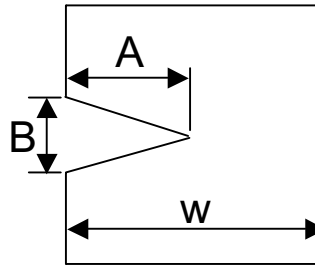
Analysis of Specimen Geometry



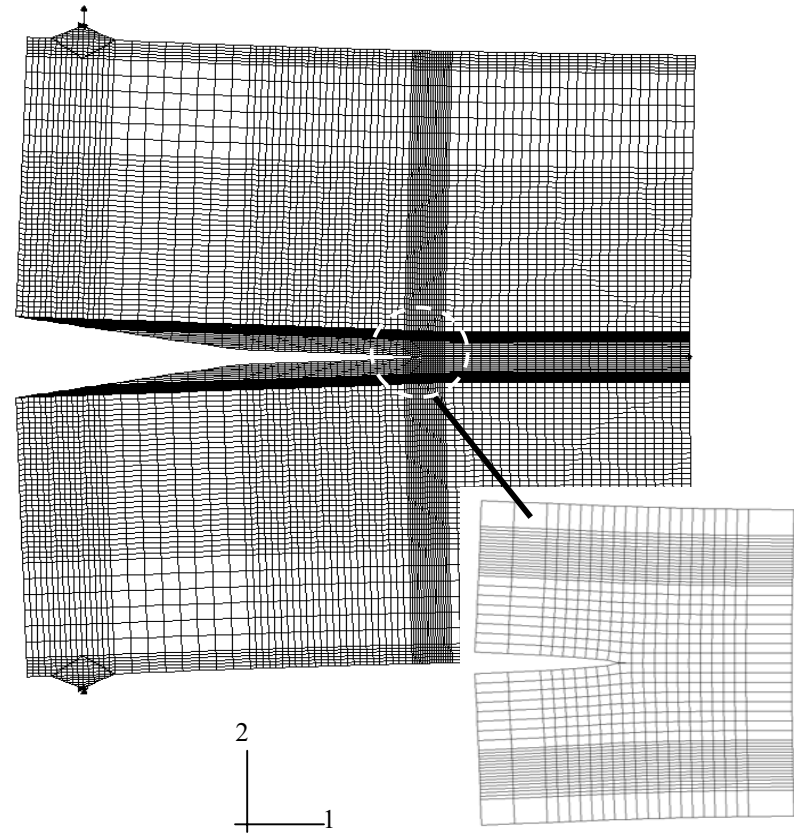
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- Determine effects of geometry on strain energy release rate and stability.
- Three specimen configurations modeled using finite elements:

1. $A=w/3$, $A/B=4$
2. $A=w/3$, $A/B=0.8$
3. $A=2w/3$, $A/B=8$



- Finite element analysis used to calculate strain energy release rates. Analysis of each configuration repeated for a range of crack lengths.
- Relationship between strain energy release rate and crack length assumed the same in tension and compression.



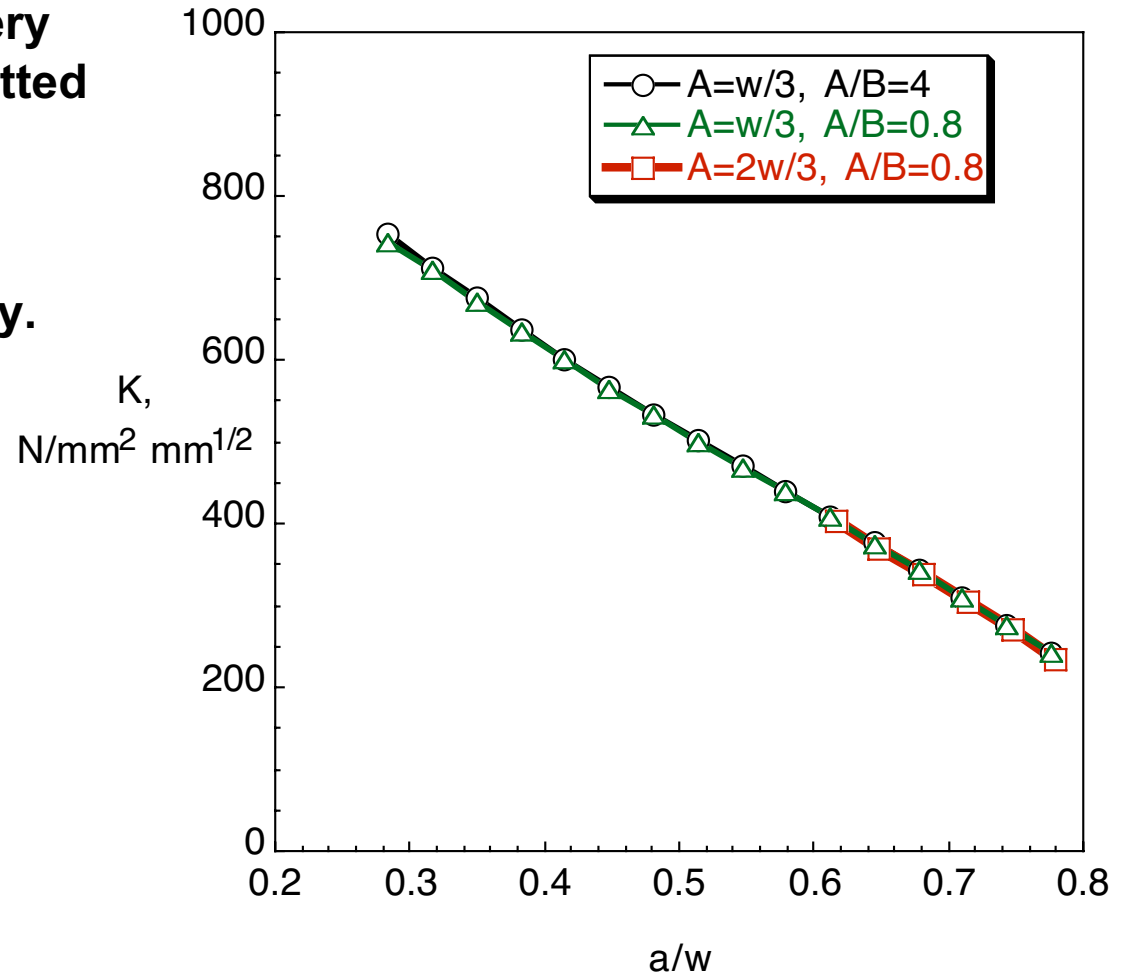
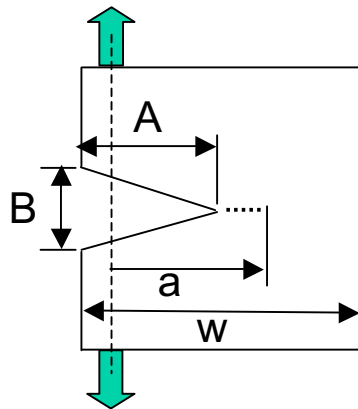


Finite Element Results



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- All configurations have very similar K curves when plotted as a function of “ a .”
- Notch geometry does not significantly affect stability.
- Geometry selected:
 $A = w/2$, $A/B = 2$

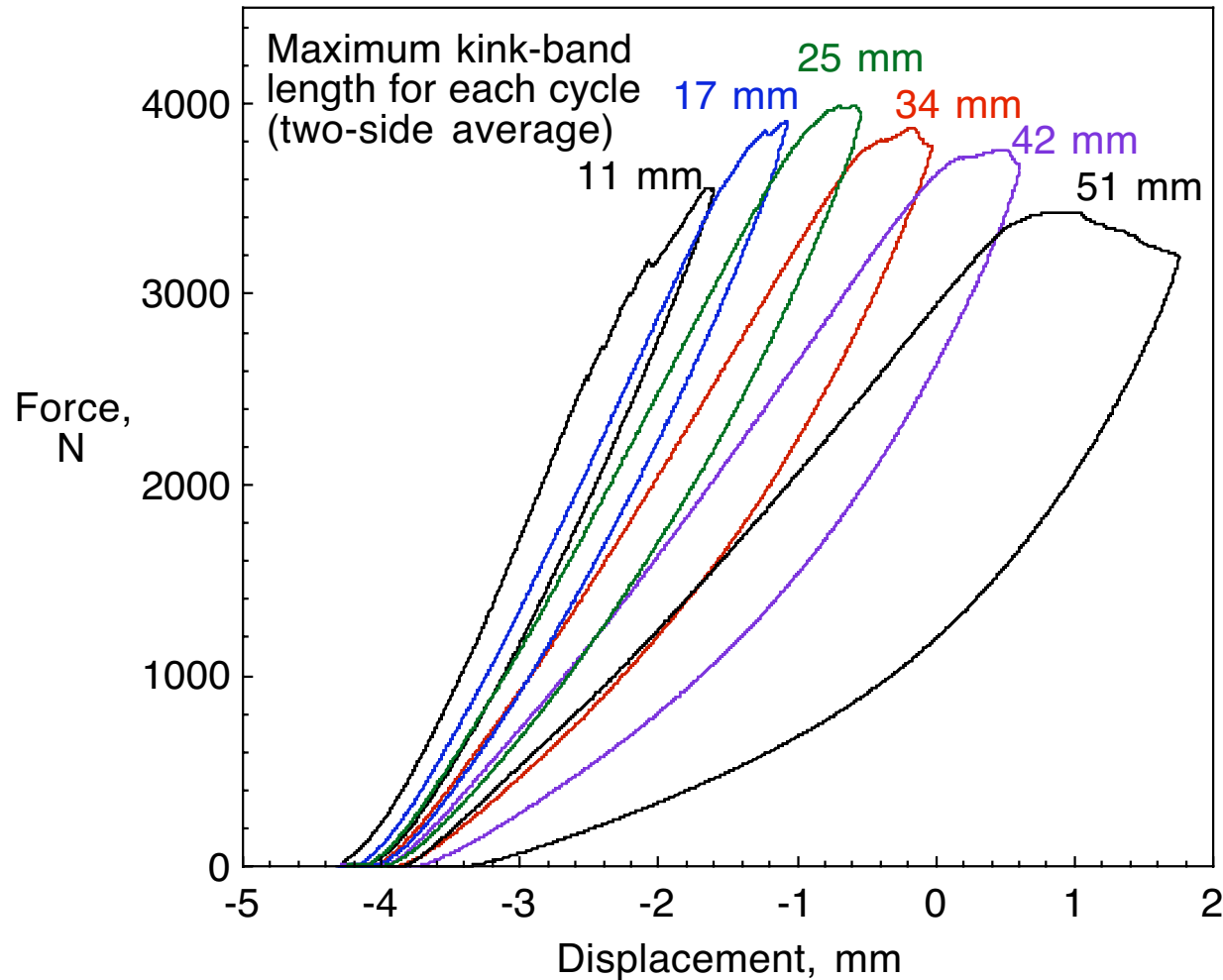




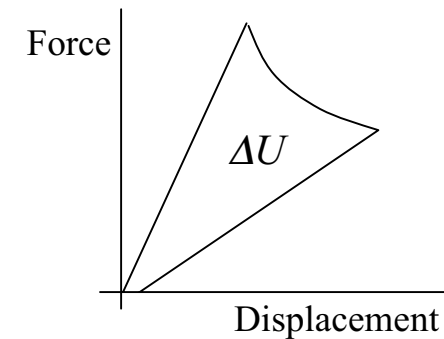
Force-Displacement Behavior



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$$G = \frac{1}{2t_f} \frac{\Delta U}{\Delta L_b}$$



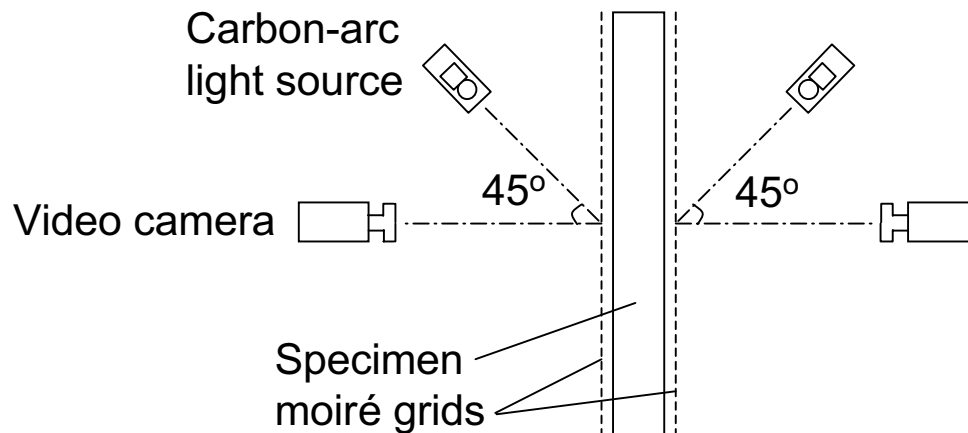


Monitoring Kink-Band Propagation



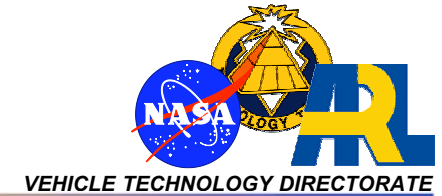
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- Shadow moiré used
- Moiré grid attached to both facesheets
- High-intensity, collimated light placed 45° to specimen
- Both sides of specimen monitored (recorded on video)

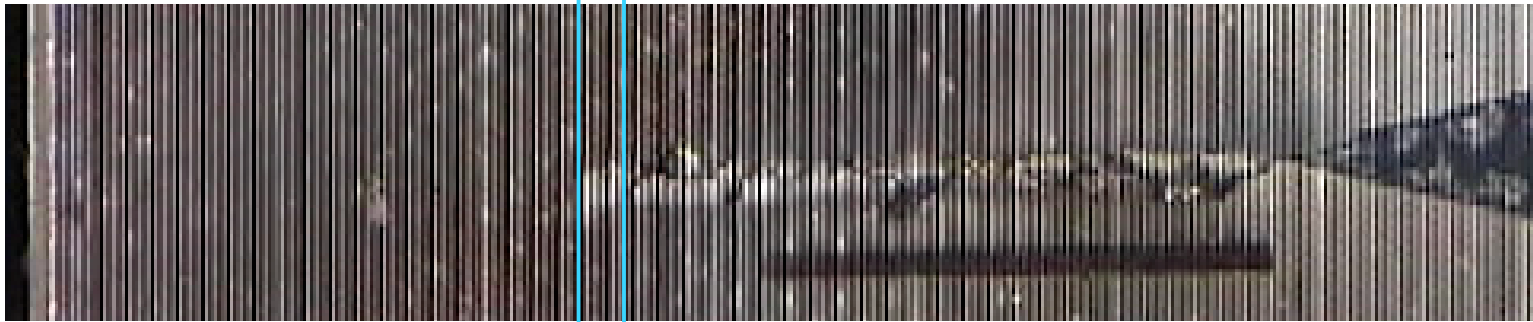




Comparison of Techniques to Determine Kink-Band Lengths



Shadow
Moire



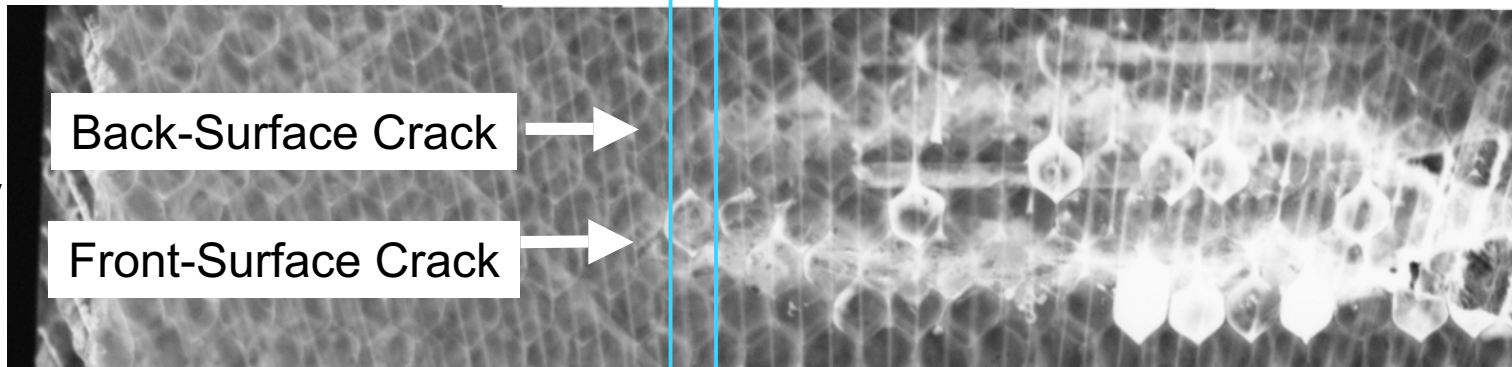
Surface
Photo



X-Ray

Back-Surface Crack →

Front-Surface Crack →

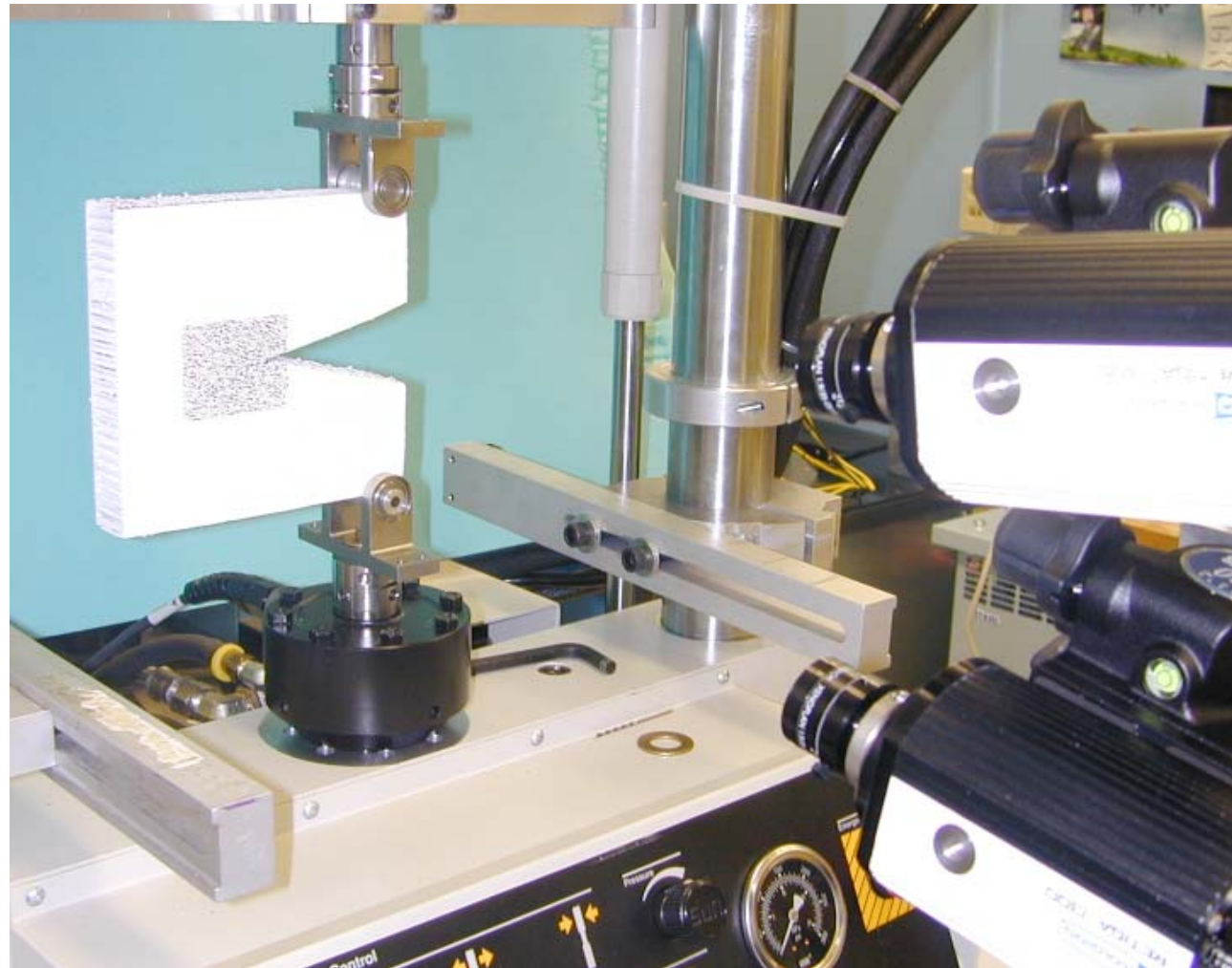




Optical Deformation Measurements

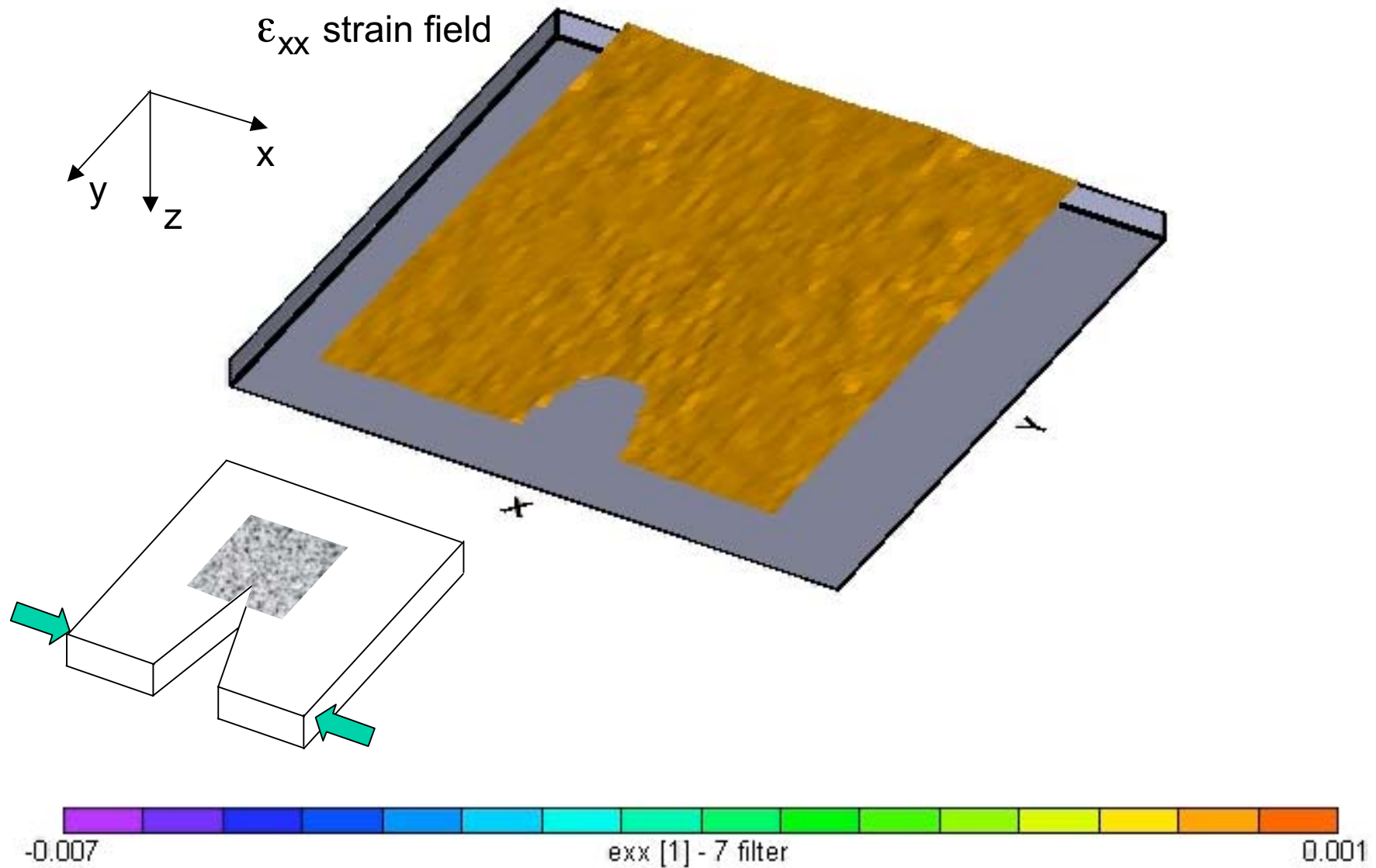


- **Measurements taken in speckled region**
- **One image recorded every 10 seconds**
- **All strains were calculated from an image of an unloaded specimen prior to the first load application**





Strain Field Animation





Compact Compression Test Matrix



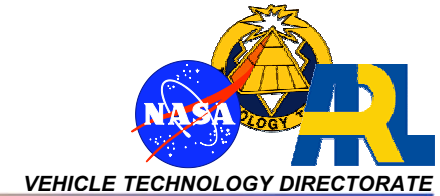
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- **Objectives:**
 - Evaluate specimen and test methodology
 - Generate data for CAI strength predictions
 - Investigate the effects of material and layup
- Plain-weave carbon fabric facesheets (3-6 plies)
- Nomex honeycomb

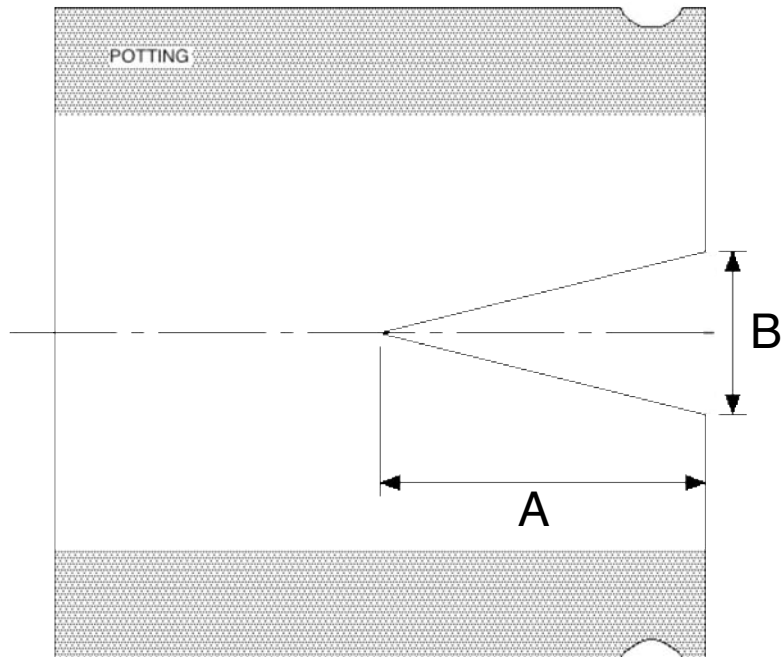
Config	Material System	Facesheet Layup	Core Thickness
a	1 (toughened epoxy)	$[(\pm 45)/(0/90)]_S$	25 mm
b	1 (toughened epoxy)	$[(\pm 45)/(0/90)/(\pm 45)]$	25 mm
c	2 (epoxy)	$[(0-90)/(0-90)/(0-90)_{1/2}]$	25 mm
d	3 (epoxy)	$[(0-90)/(\pm 45)]_3$	29 mm
e	3 (epoxy)	$[(0-90)/(\pm 45)]_2$	19 mm



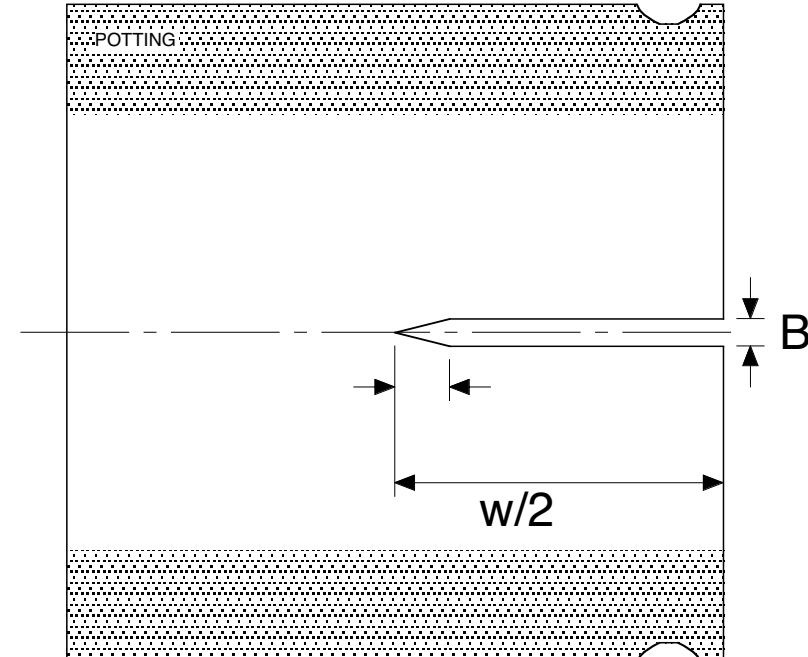
Specimen Geometry Parametric Testing



V Notch



Slot

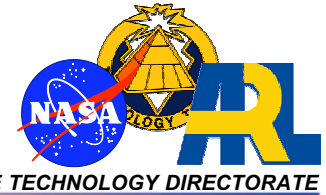


1. $A = w/2$, $A/B = 6$
2. $A = w/2$, $A/B = 2$
3. $A = w/2$, $A/B = 1.2$
4. $A = 2w/3$, $A/B = 4$
5. $A = 2w/3$, $A/B = 2$

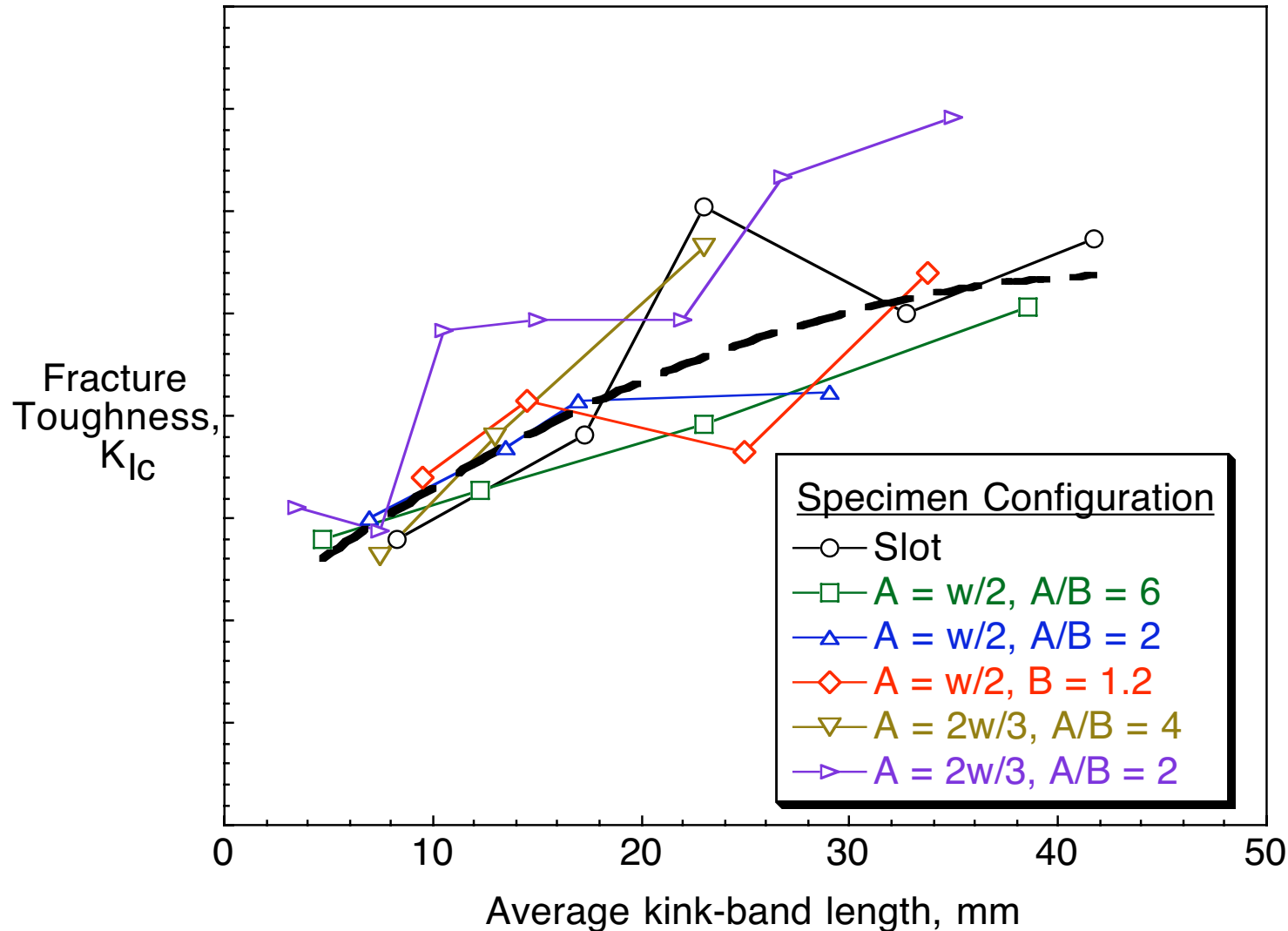
Configuration “a” used for testing



Fracture Toughness Measurements Parametric Study



$[(\pm 45)/(0/90)]_S$ (Config "a")



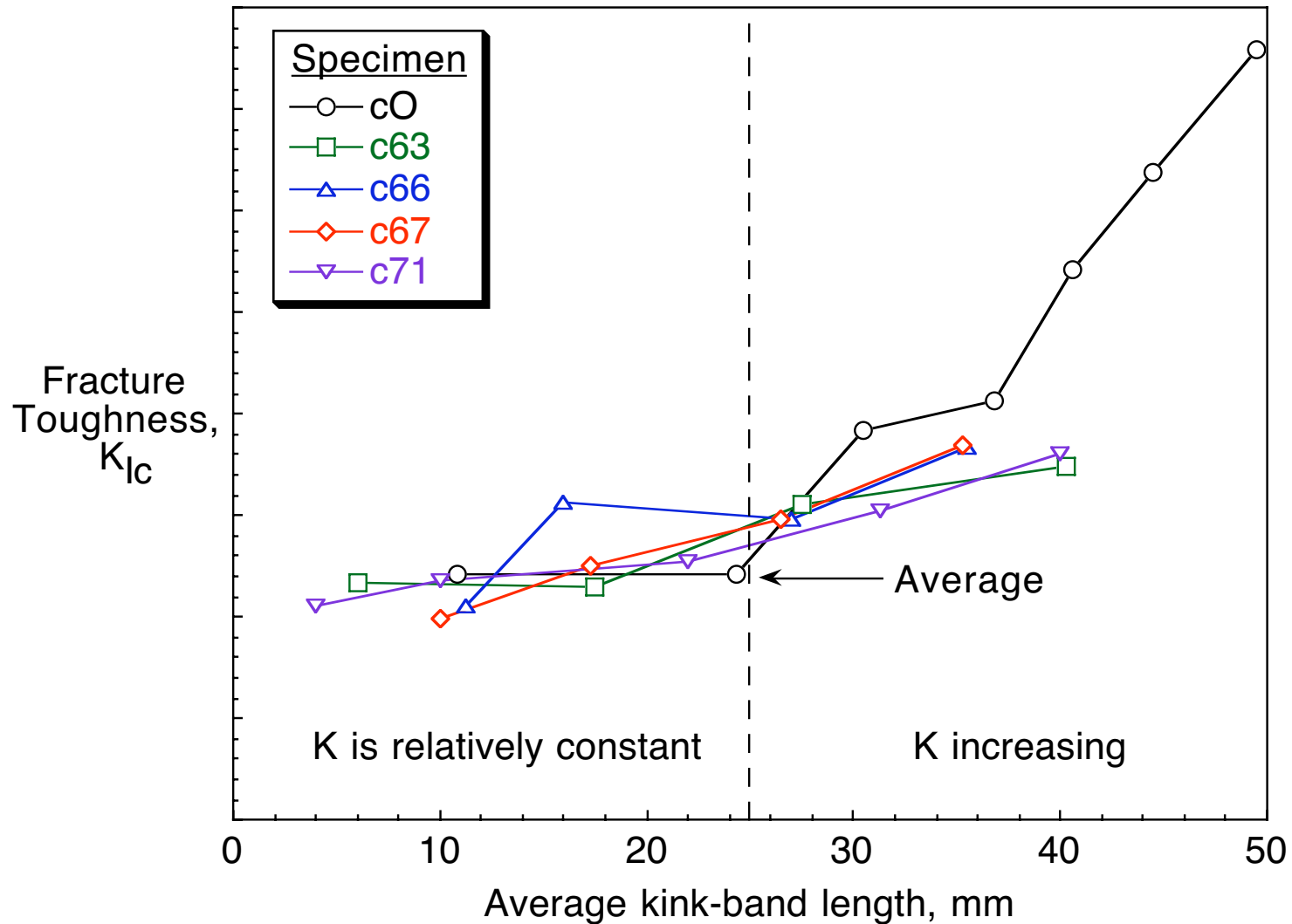


Fracture Toughness Measurements



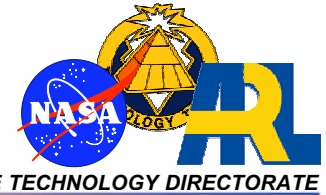
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$[(\pm 45)/(0/90)/(\pm 45)]$ (Config "b")

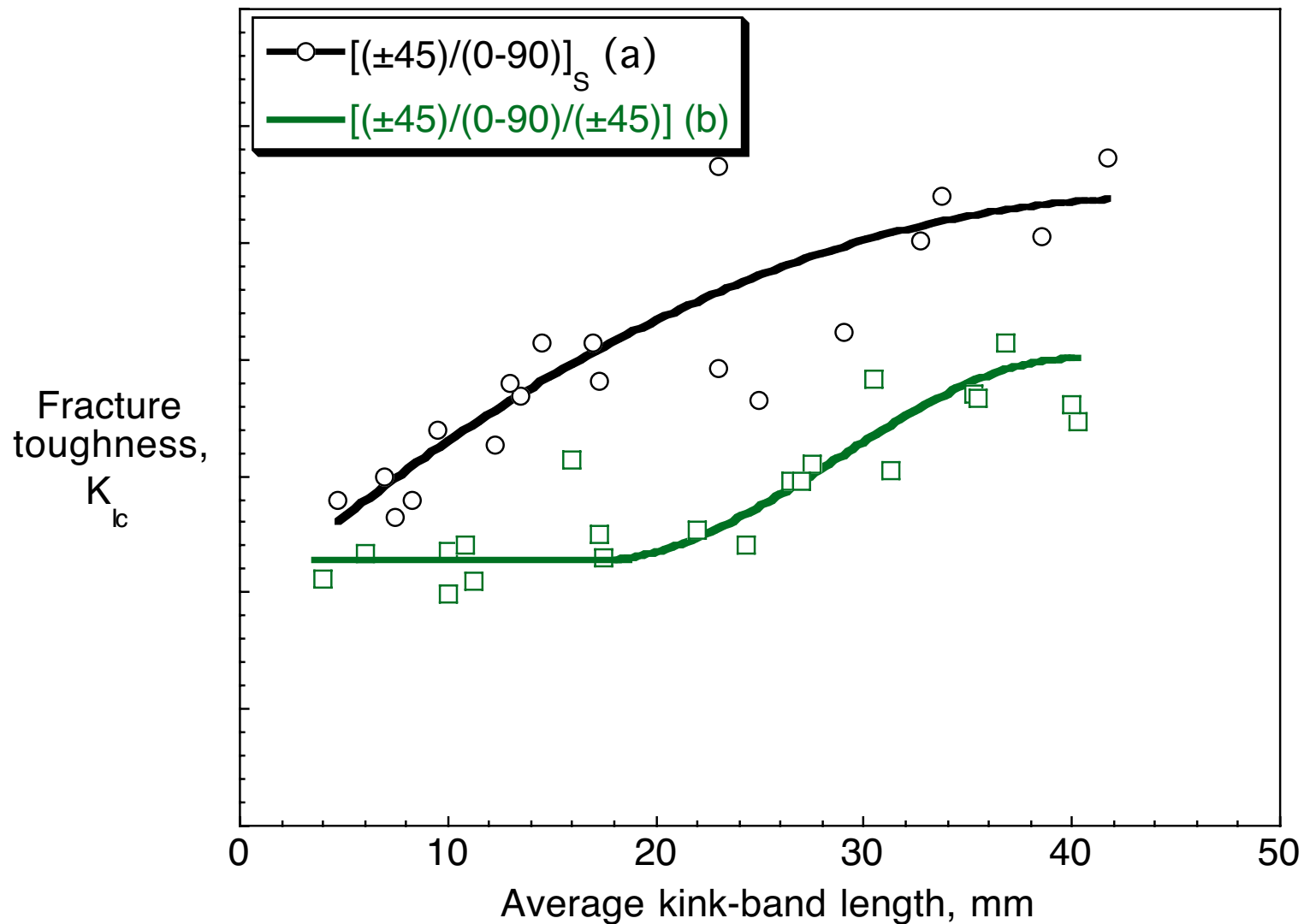




Fracture Toughness Measurements Comparison of Layups



Toughened epoxy (Material "1")

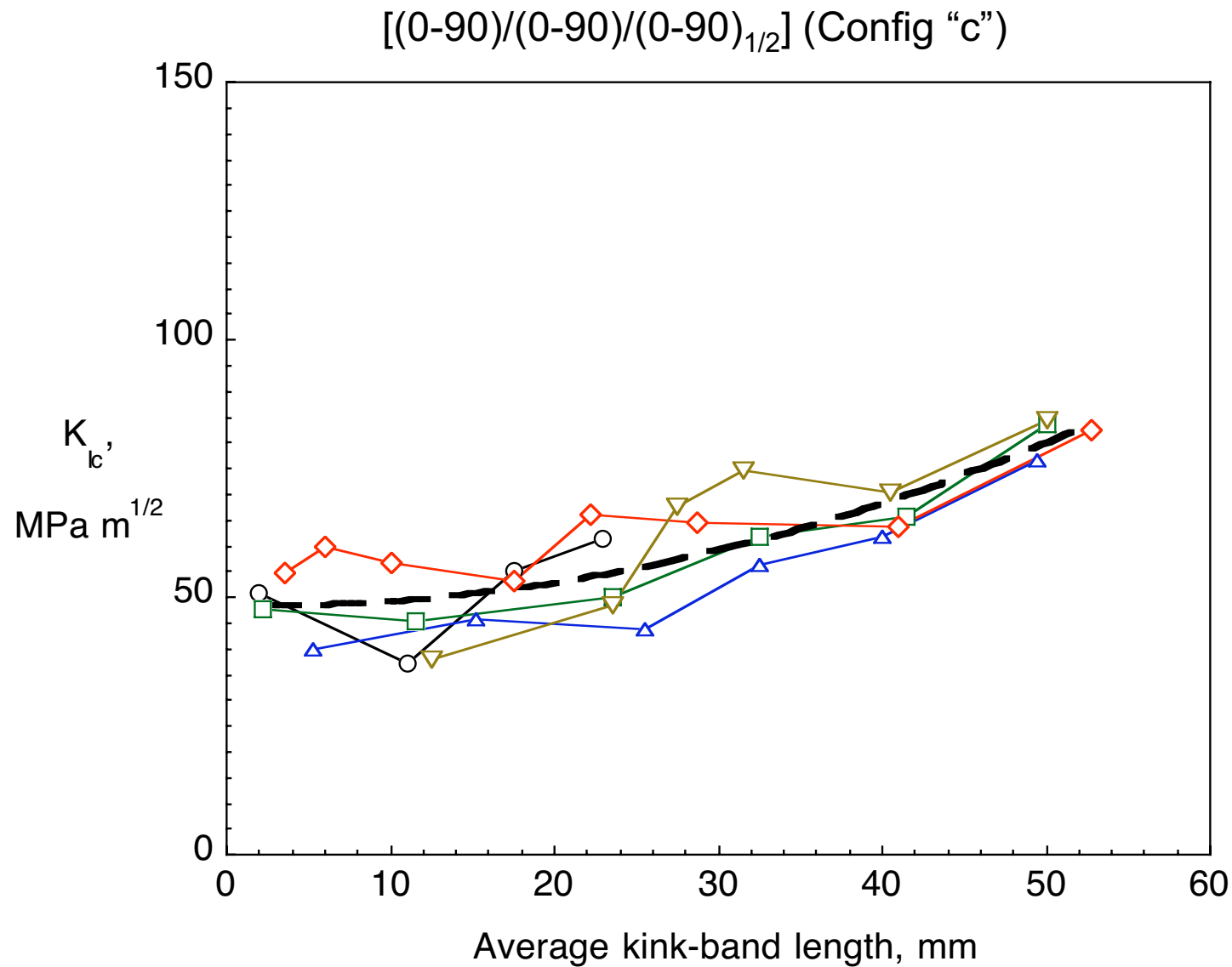




Fracture Toughness Measurements



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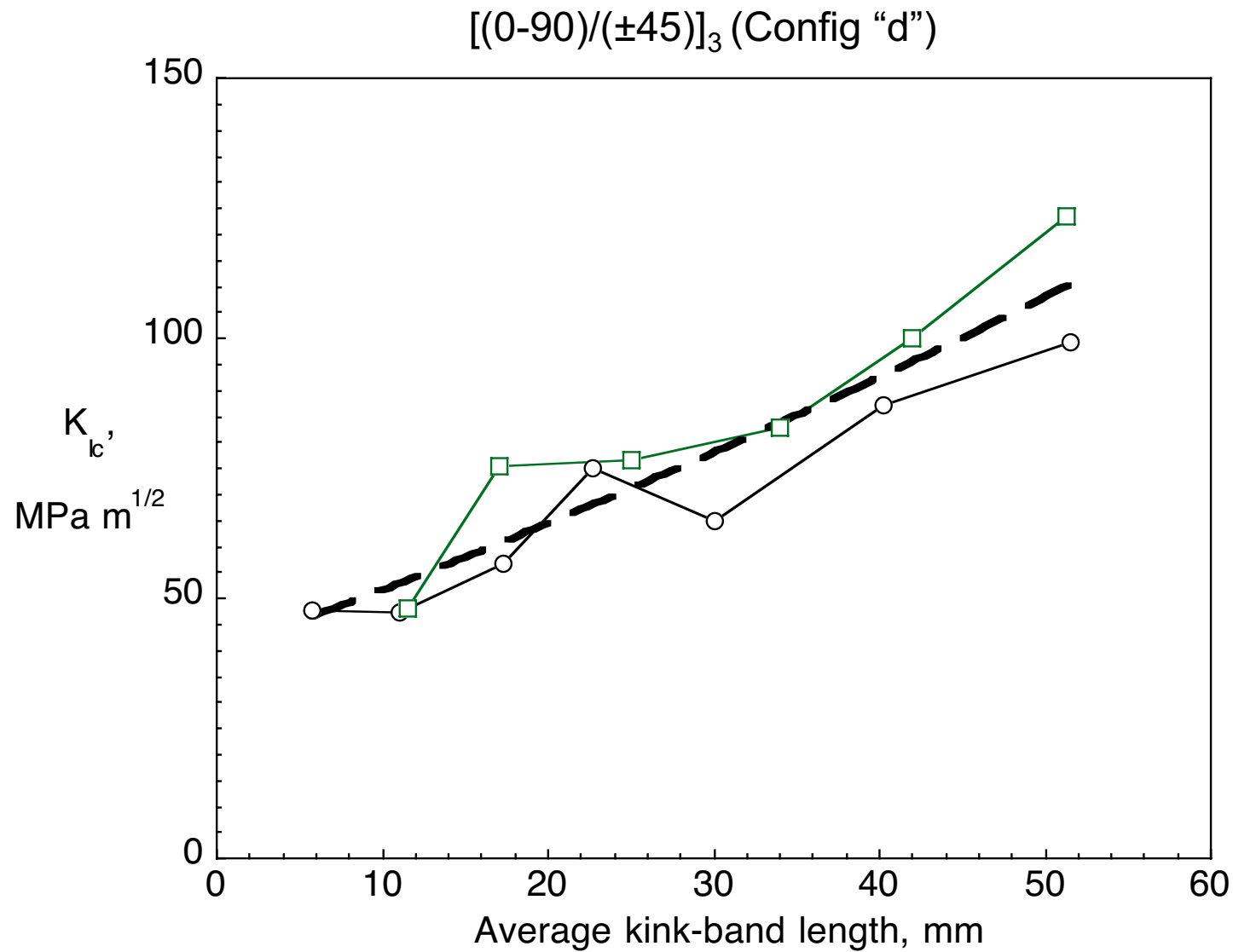




Fracture Toughness Measurements



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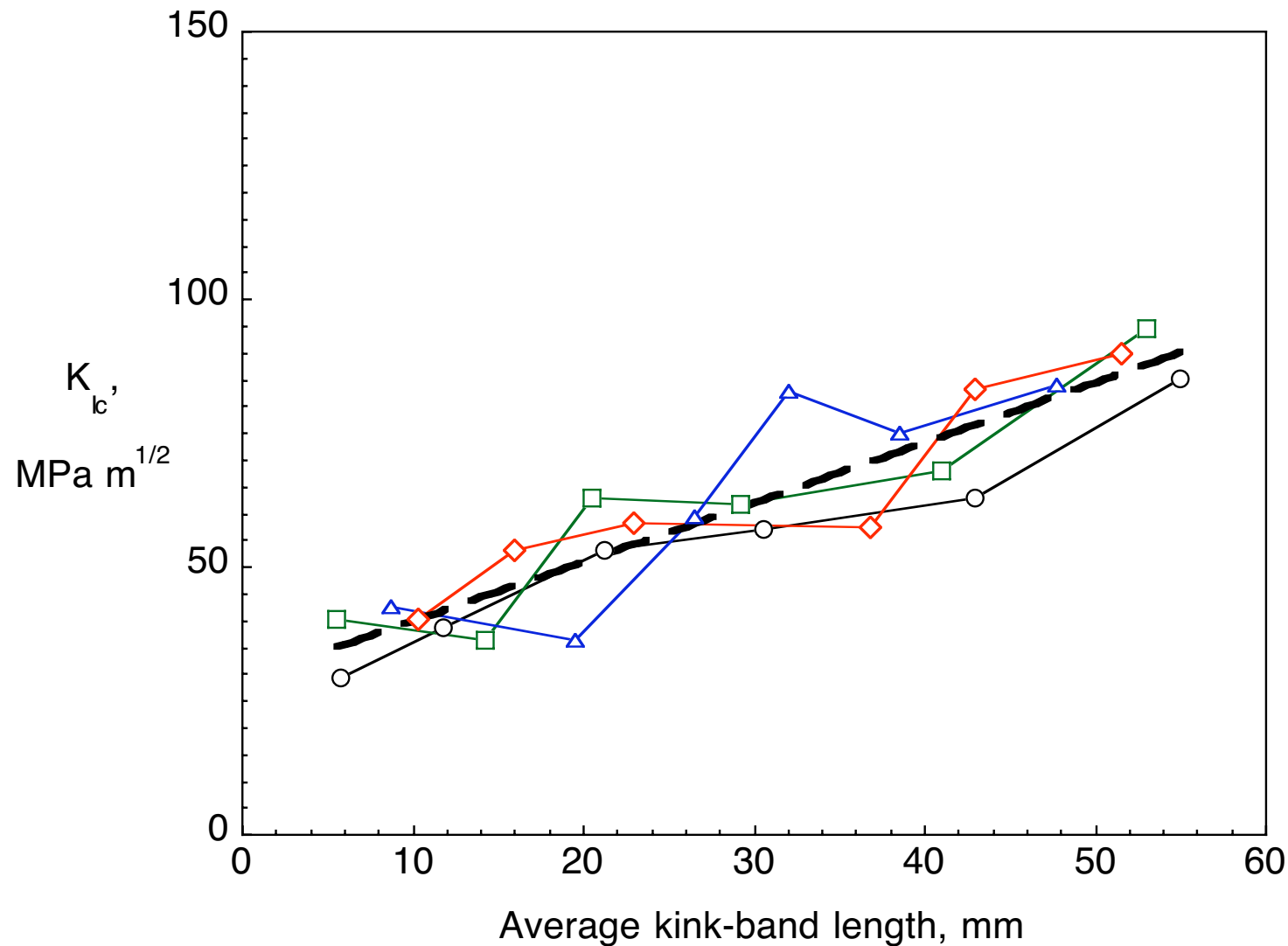


Fracture Toughness Measurements



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$[(0-90)/(\pm 45)]_2$ (Config "d")

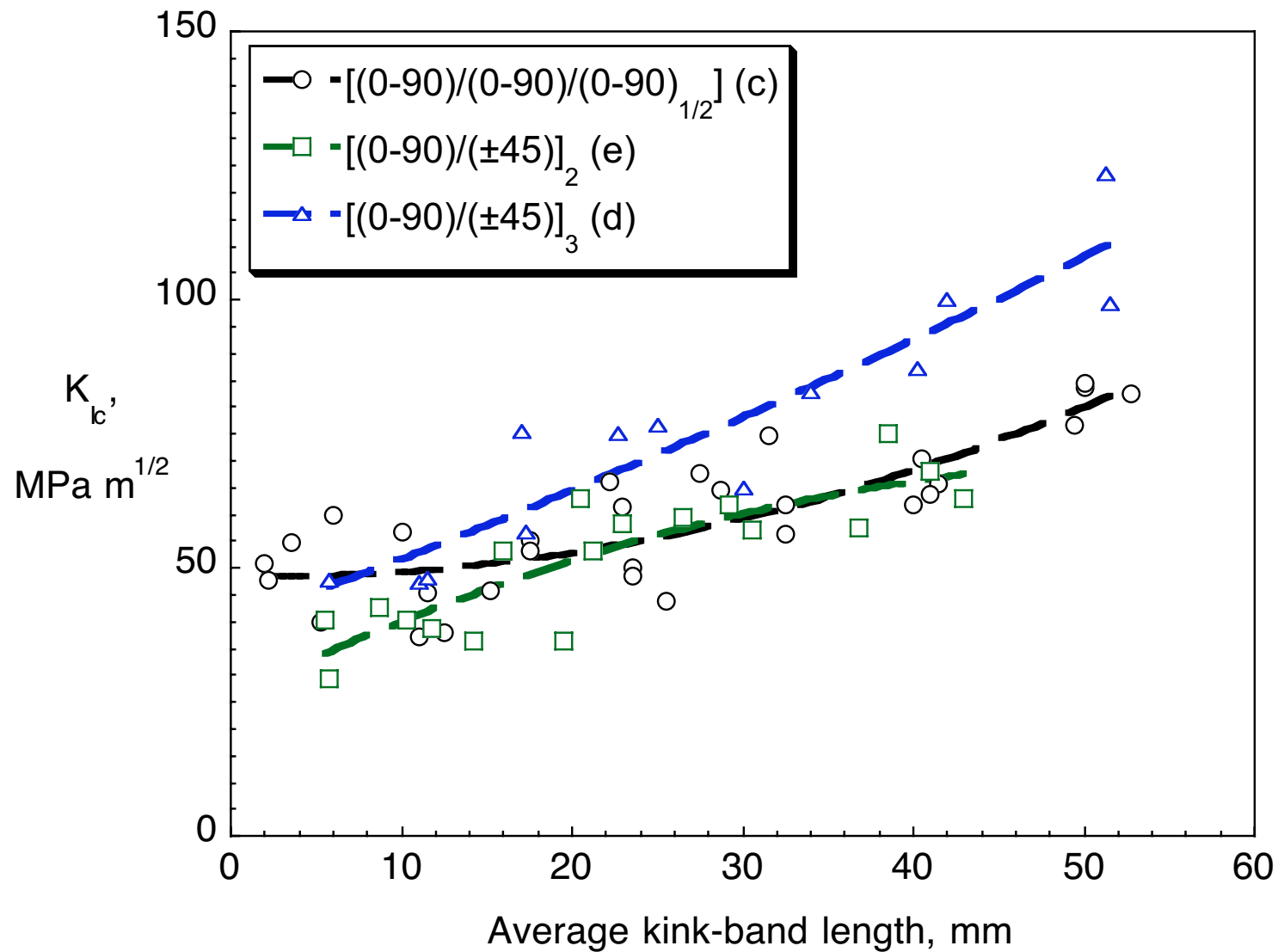




Fracture Toughness Comparison



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CONCLUDING REMARKS



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- Developed new test to obtain facesheet fracture toughness, K_{Ic} , needed for CAI strength predictions.
- Replicates kink-band growth observed during CAI testing.
- Captures energy dissipation associated with kink-band growth.
- Fracture energy measurements were not affected by specimen geometry.
- Fracture energy observed to increase with kink-band length.
- Lower bound values of K_{Ic} should be used to yield conservative CAI strength predictions.
- Scatter in fracture energy measurements does not significantly affect CAI strength predictions.
- Measured fracture energy was a function of facesheet thickness/layup (laminar property).



ACKNOWLEDGEMENTS



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