

Composite Materials Specimen Design for Validation of an Energy-Based Multi-Axial Characterisation Methodology

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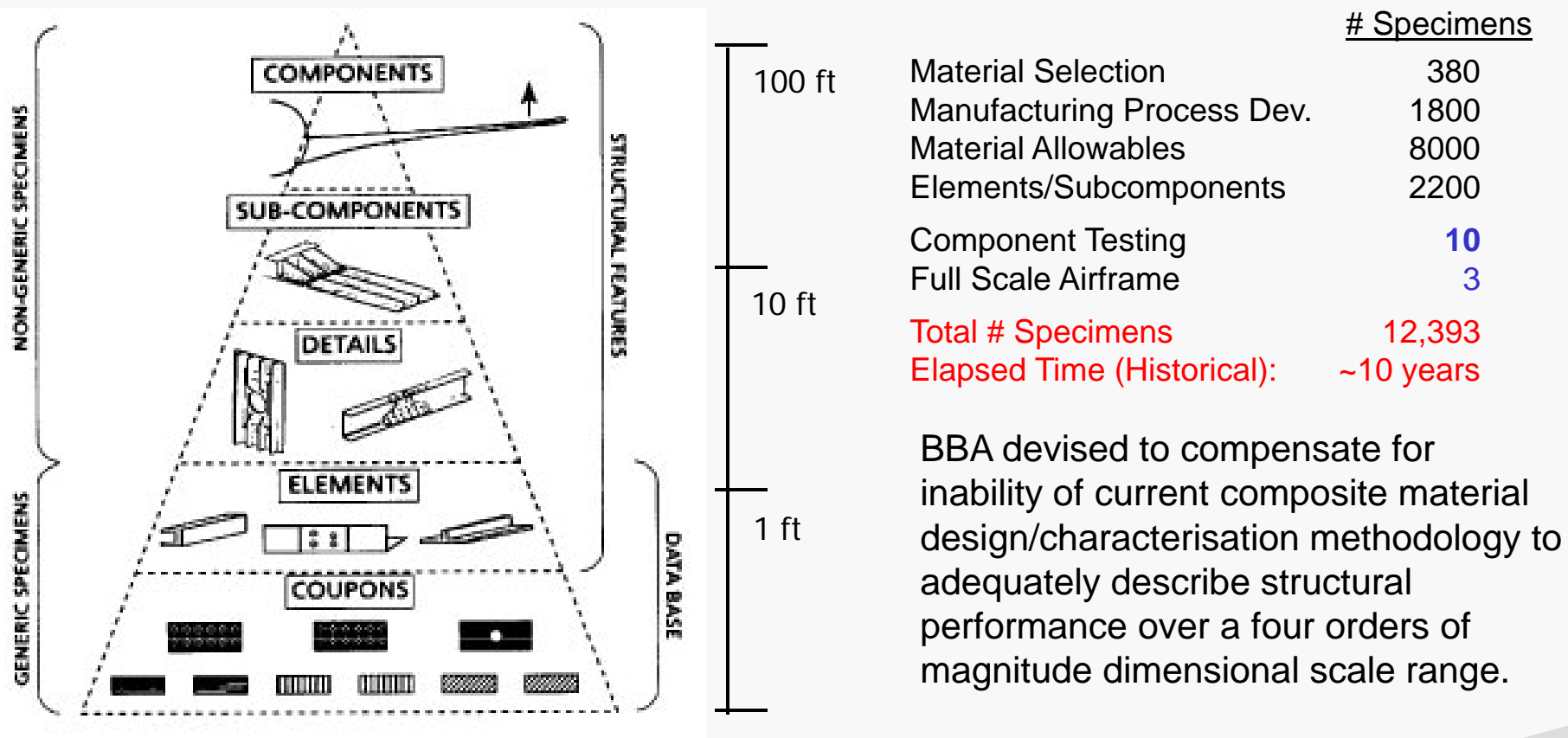


Overview

- Motivation
- Length Scale
- Multi-Axial Characterisation
- Validation Specimen Design
- Summary

Motivation: Economics

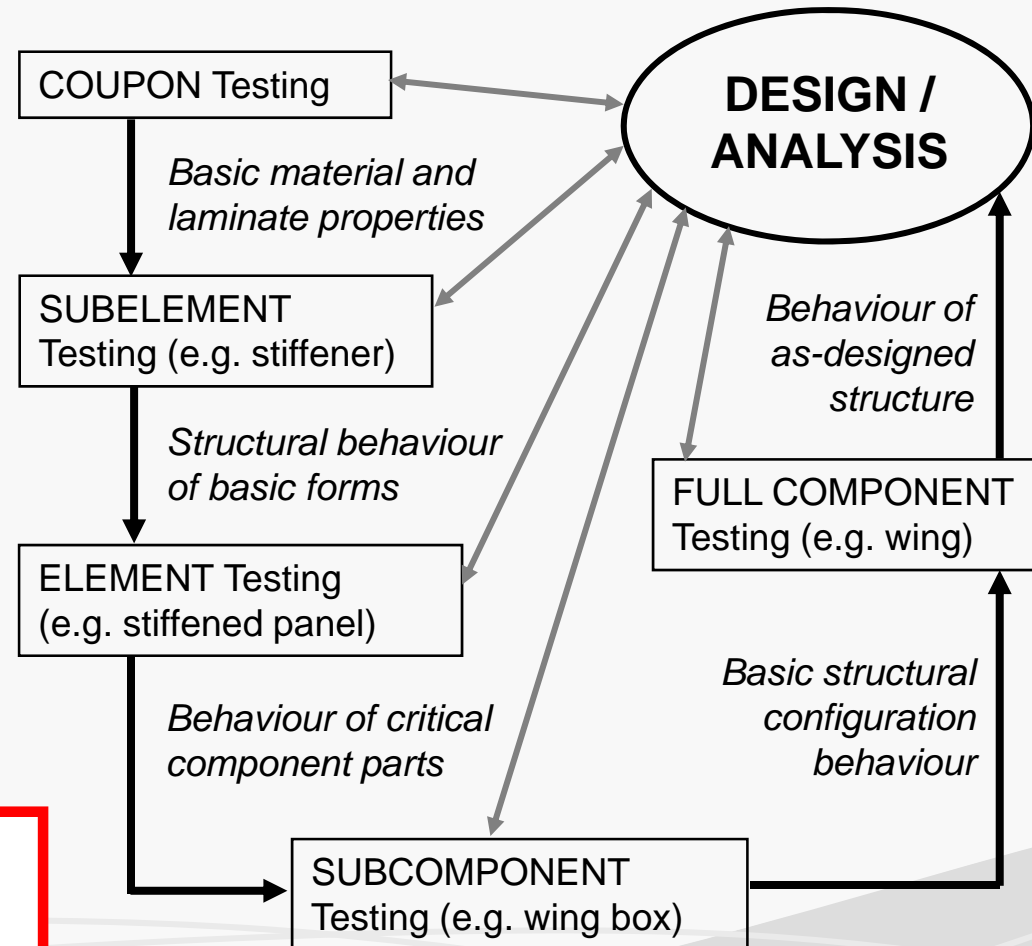
- CMH-17 Building Block Approach (BBA) Pyramid of Tests



BBA is based on single-axis testing that requires extrapolation to real-life loading scenarios, leading to further cost and design conservatism

Length Scale

- Current design/analysis
 - Extensive testing utilised to establish material “allowable stresses” and other parameters
 - Mechanism-based models exist in isolation at several scales
- Parameters transferred to progressively higher levels of structural complexity
 - Knockdown factors
 - Various empirical and semi-empirical approaches
 - Models are unlinked and do not account for damage mode and length scale interactions
- A one-way process with little chance for iteration



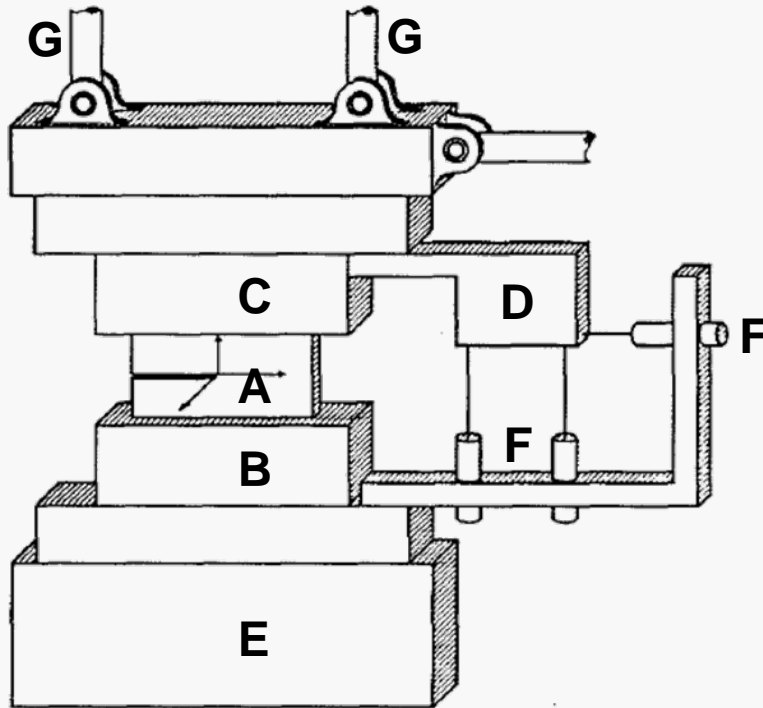
Inability to address length scale issues is a key driver for the high cost of BBA

Multi-Axial Characterisation

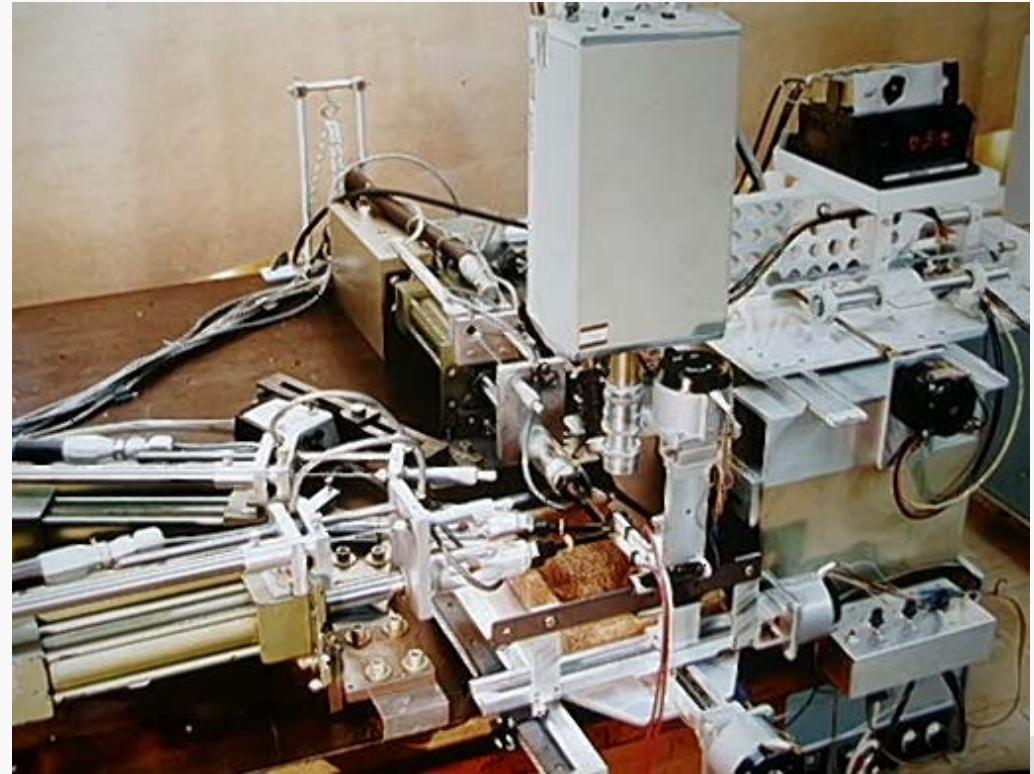
- Multi-axial loading machines developed to apply combined loading on characterisation specimens
- Different combinations of combined loading are applied in order to sample the loading space
- Loading machines are highly automated and involve complex robotic actuators and sensors
- Data processing involves manipulation of massive amounts of data

Multi-Axial Characterisation

- 1970: NRL developed 3-DOF (in-plane) loader

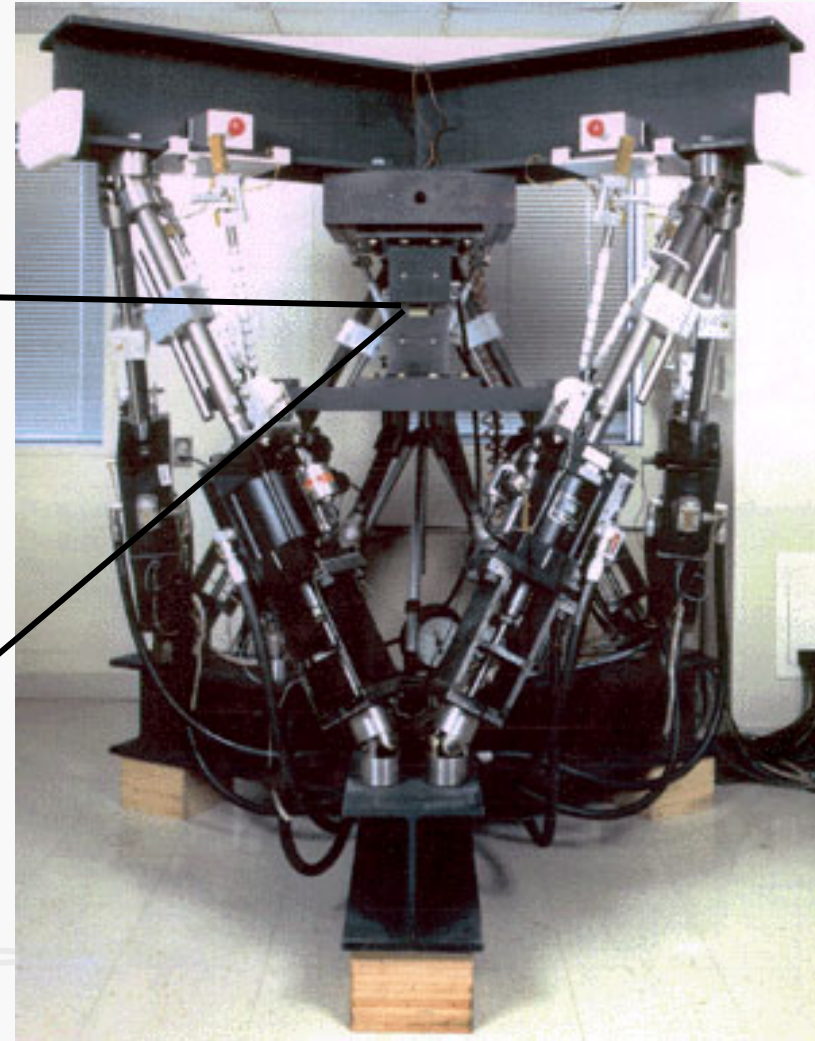
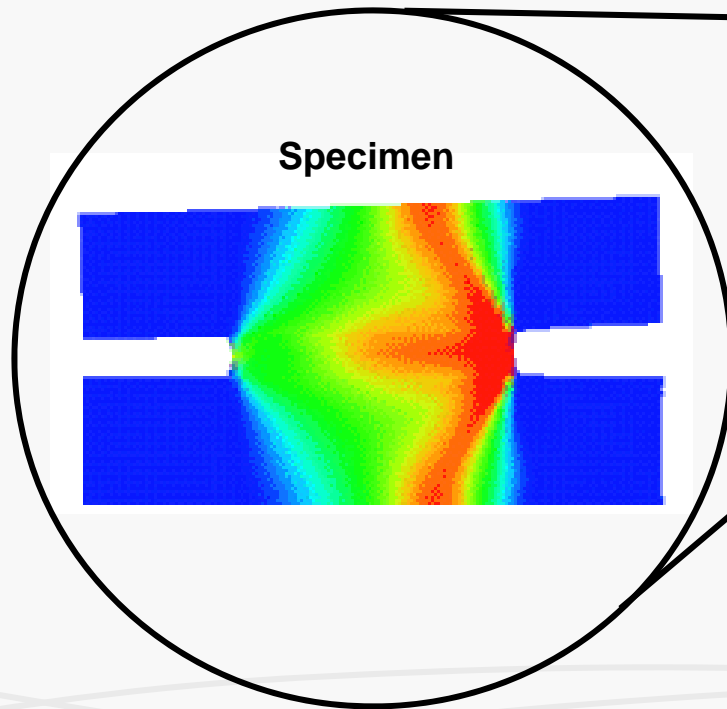


- | | |
|--------------------------|--------------------|
| A: Specimen | E: 3D loading cell |
| B: Fixed grip | F: DCLVDT |
| C: Moveable grip | G: Actuator |
| D: 6-D DCLVDT transducer | |



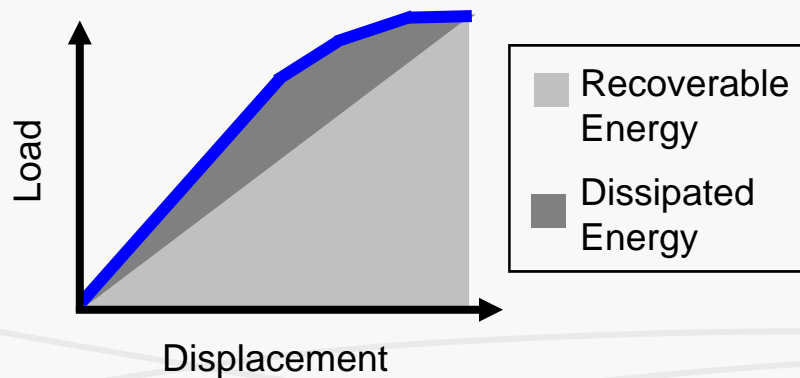
Multi-Axial Characterisation

- 6-DOF loader based on hexapod frame



Multi-Axial Characterisation

- Multi-axial characterisation approach is based on the concept of Dissipated Energy Density (DED)
 - DED can be determined experimentally from nonlinear behaviour
 - Nonlinearity associated with irreversible damage processes
 - DED function (ϕ) obtained to relate strain to DED
 - DED function incorporated into nonlinear material constitutive law



COMPUTE COEFFICIENTS OF ϕ THAT MINIMISE THE SYSTEM OF EQUATIONS DERIVED FROM THE ENERGY BALANCE:

$$\int_0^{u_r} t_u q_v dq^v - \frac{1}{2} t_s u_i u^v = \int_{\partial V} \phi(\varepsilon_i(x_j)) dx_j$$

Applied Energy Recoverable Energy Dissipated Energy

ADEPT

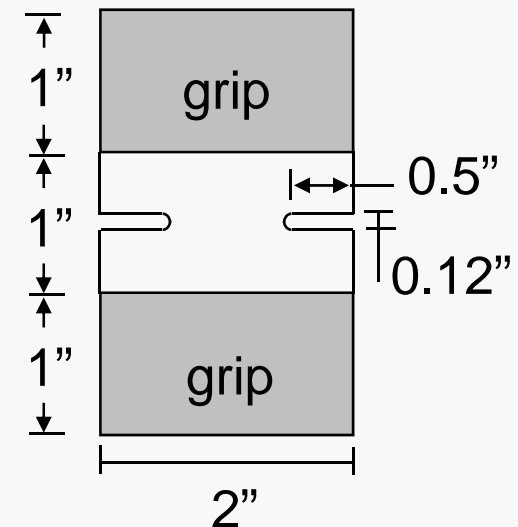
- “Application of **D**issipated **E**nergy Density to com**P**osite s**T**ructures”
- Four-year collaborative research project (2006 – 2010)
- Objectives:
 - Build upon and extend the NRL data-driven multi-axial material characterisation approach to develop a cost-effective methodology (compared to BBA) for the determination of mechanical behaviour in complex composite structures subjected to realistic loading conditions
 - Validate the methodology through testing on coupons and substructures at ambient conditions with a focus on issues of length scales manifested across this range
 - Develop an overall approach to couple the methodology with commercial software for calculating stress state and assessing overall structural behaviour

Validation Specimen Design

- Specimens need to be designed for testing at a range of different length scales
 - Characterisation
 - Open Hole Tension specimens
 - Ply drop
 - Stiffened panel
- Goal of testing is to achieve two convergent aspects
 - Investigate key length scale effects experimentally
 - Characterise failure at each length scale
 - Validate analysis methodology
 - Understand how to link between scale levels

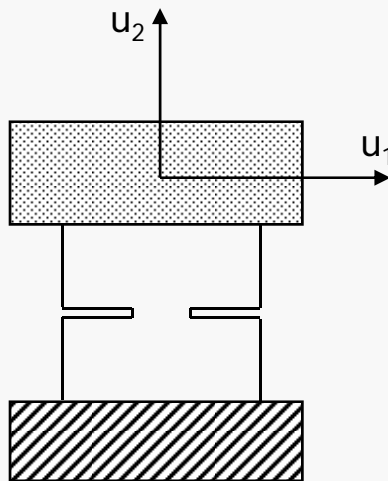
Characterisation Specimens

- Size: Based on limits of 6-DOF loader
 - Grip size, failure load
- Disturbance of strain field → Notch
 - Ensure failure in gauge region
- Symmetry preferred → Double Notch
- Lay-up based on $[\theta, -\theta]$
 - Lay-up based on previous work on characterisation methodology
 - Coupling effect (asymmetry) required for 3D characterisation
 - Ply thickness constant for all layers
- Scale effects: $[\theta, -\theta]_{16}$ and $[\theta_4, -\theta_4]_4$

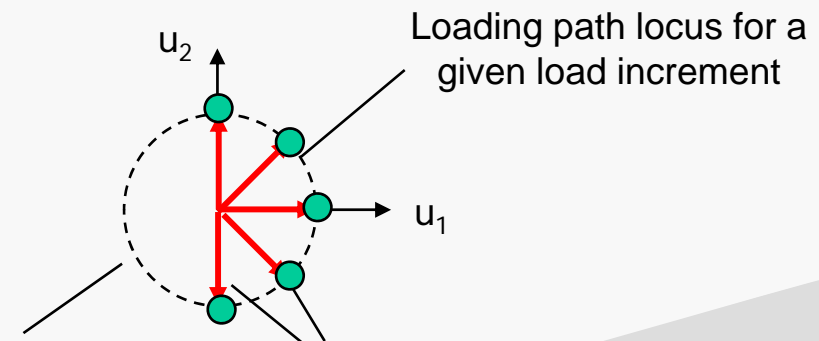


Characterisation Specimens

- Total number of specimens controlled by number of individual loading paths
- Current sampling scheme is uniform, and exploits symmetry



2-DOF
5 loading paths



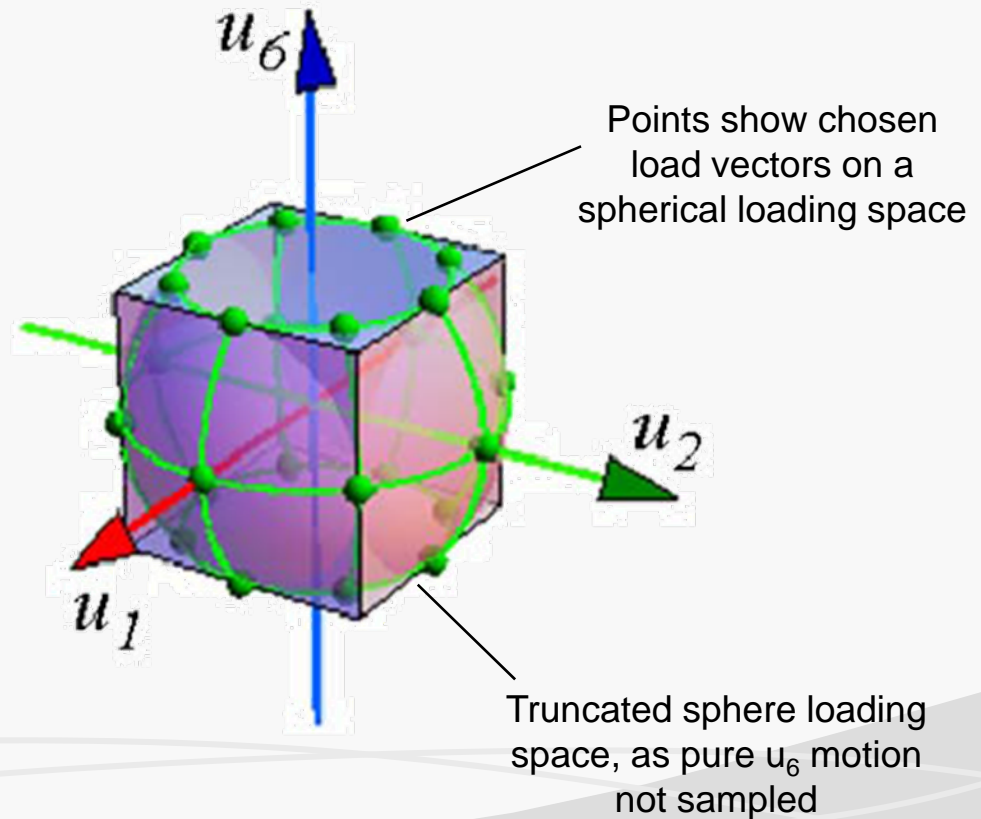
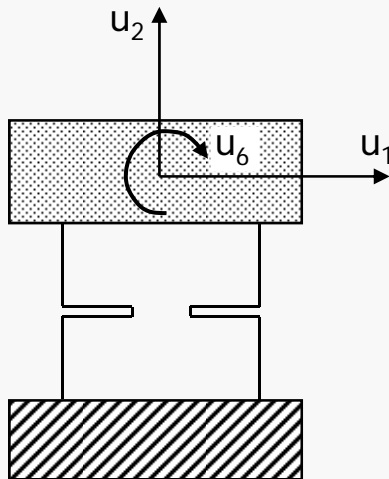
Symmetry exploited,
as -ve and +ve u_1
vectors are identical

**load vectors sample
load space evenly**

Characterisation Specimens

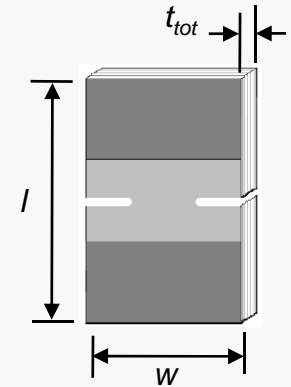
3-DOF

24 loading paths



Characterisation Specimens

- Number of specimens also controlled by:
 - Number of different angle ply lay-ups, $[+\theta, -\theta]$
 - Number of changes in length scale
 - Length, width and total thickness of specimen
 - Ply thickness



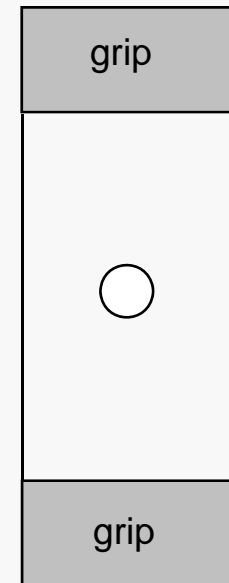
- Separate task looking at using a reduced scheme
 - Define metrics for quality of data, use to optimise load vectors, both off-line and on-line planning

Characterisation Specimens

- Current project uses a 4-DOF space:
 - Number of paths = 72
 - Number of lay-ups = 4 (from two plates)
 - Number of scale effect variations = 2 (ply thicknesses)
 - Number of repetitions of each specimen = 2
- Characterisation requires 1152 specimens
 - $144 \times [15, -15]_{16}$
 - $144 \times [30, -30]_{16}$
 - $144 \times [60, -60]_{16}$
 - $144 \times [75, -75]_{16}$
 - $144 \times [15_4, -15_4]_4$
 - $144 \times [30_4, -30_4]_4$
 - $144 \times [60_4, -60_4]_4$
 - $144 \times [75_4, -75_4]_4$

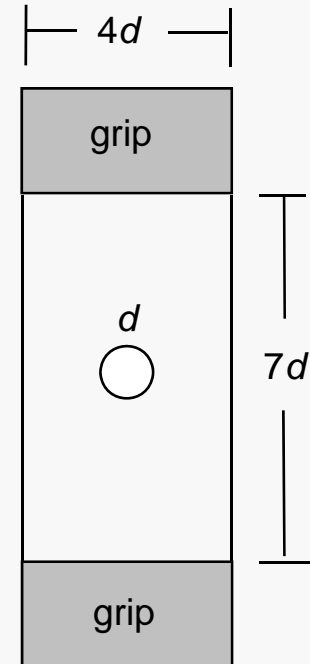
Open Hole Specimens

- OH for validation at coupon level using a standard specimen
- Goal to represent real structural details, (e.g. bolted joint)
- Scale effects drives specimen design
 - “In-plane” scaling of geometry (length/width)
 - Ply thickness at two variations
- Possible to investigate open hole specimen in tension and bending to get tension/compression behaviour



Open Hole Specimens

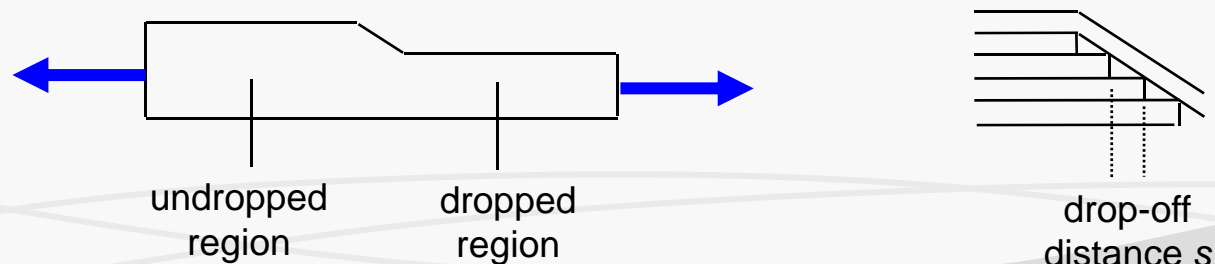
- Size of hole necessary to constitute a significant structural detail
 - 0.5" and 1.0" hole sizes selected
- Edge distances set based on hole diameter
- Lay-up based on $[45,0,-45]$
 - 90° not used to prevent excessive transverse cracks
- Scale effect: $[45,0,-45]_{4S}$ and $[45_4,0_4,-45_4]_S$
- 36 specimens
 - $d = 0.0$: $6 \times [45,0,-45]_{4S}$, $6 \times [45_4,0_4,-45_4]_S$
 - $d = 0.5$: $6 \times [45,0,-45]_{4S}$, $6 \times [45_4,0_4,-45_4]_S$
 - $d = 1.0$: $6 \times [45,0,-45]_{4S}$, $6 \times [45_4,0_4,-45_4]_S$



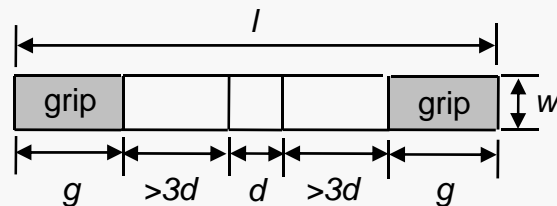
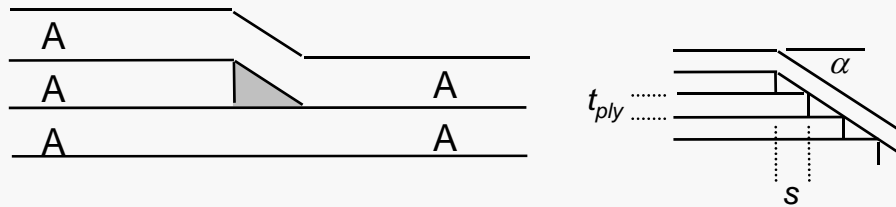
$d = 0.5", 1.0"$

Ply Drop Specimens

- Ply drop for validation at another structural detail
 - Out-of-plane stresses feature prominently
 - Ply drops are common in design and a key type of structural detail
- Ply drops generate interlaminar stresses due to two main effects
 - Termination effect: Load transfer from undropped to dropped region
 - Offset effect: Load mismatch between two regions
- Additional interlaminar and transverse stresses due to:
 - Poisson's mismatch: Strain mismatch between two regions
 - Angle mismatch between plies
- Use of ply drop specimens
 - Promote out-of-plane failure mechanisms
 - Capture effects related to this specific structural detail



Ply Drop Specimens

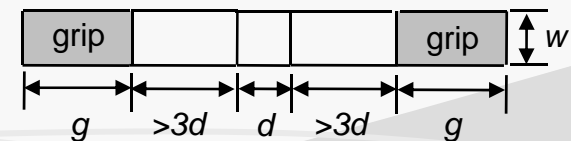
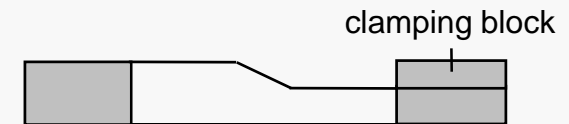
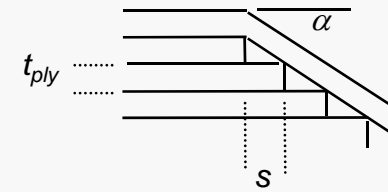
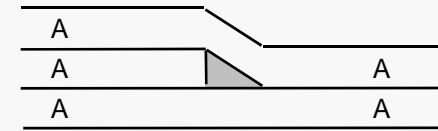


- A is a sublaminate block of 12 plies $[45,0,-45]$
 - $[45,0,-45]_{2S}$
 - $[45_2,0_2,-45_2]_S$
- $t_{ply} = 0.005''$
- $t_u = 36t_{ply} = 0.18''$
- $s = 0.04''$, $\alpha = 7.4^\circ$
- $d = 12s = 0.5''$
- $g = 2''$ (set by machine)
- $l > 7d + 2g = 8''$
- $w > 3d = 1.5''$

- 12 specimens
 - $6 \times A = [45,0,-45]_{2S}$
 - $6 \times A = [45_2,0_2,-45_2]_S$

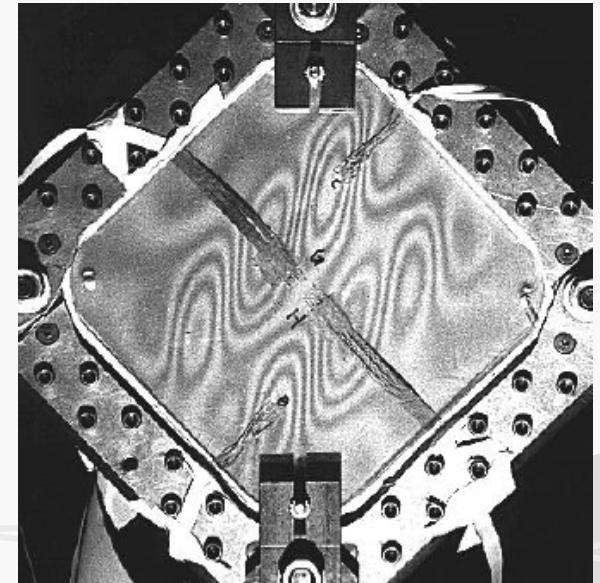
Ply Drop Specimens

- Aim to represent a “real” configuration
 - proportion of dropped plies set to 33%
- Laminate based on A-block sub-laminate
 - Allow for drop-off of a laminate block
 - Allows for ply thickness effects to be studied
 - Overlamine minimises interaction with edge stresses
 - 90° plies removed to prevent excessive matrix cracking
- Ply drop-off length, s
 - Aim for ply drop angles, α , around 10-20 for significant out-of-plane effects
 - However, want to drop-off 1 ply at a time, to avoid creating another length scale
 - Minimum practical distance that plies can be placed with accuracy is 1 mm,
 - so $s = 1 \text{ mm (0.04")}$
- Specimen lengths:
 - Drop-off region, d , set by length to drop off 12 plies
 - Dropped and undropped region at least $3d$ to minimise interaction with grips
 - Grip dimension (g, w) comparable to specimen width to avoid edge effects



Stiffened Panel

- Stiffened panel for substructure validation
- Representative of typical aerospace structure
 - Postbuckling control surface
- Three blade stiffeners co-cured to thin skin
- Lay-up:
 - Skin: quasi-isotropic [25/50/25]
 - Stiffener: [37.5/50/12.5]
- Panel loaded in shear in picture frame rig
- Number of panels to be determined



Summary and Outlook

- Multi-axial characterisation approach being pursued to represent realistic loading conditions
 - Approach is based on concept of dissipated energy density
 - Data-driven, highly automated, multi-dimensional characterisation
- Length scale issues a key focus in order to address shortcomings of the building block approach
- Validation specimens designed based on:
 - Experimental investigation of length scale effects
 - Assessment of suitability of multi-axial characterisation
- Specimen manufacture underway, testing expected to start late 2008 / early 2009
- Validated methodology to be part of a cost-effective characterisation approach, incorporated within a commercial software tool

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Thank you

Questions?



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