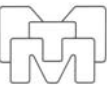


# **Experimental methodology and finite element analysis for damage studies in textile composites**

**Stepan V. LOMOV**

*Department MTM, Katholieke Universiteit Leuven*



*The presentation reports collaborative research results of:*

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Dmitry Ivanov  
Stepan Lomov  
Thanh Truong Chi  
Katleen Vallons  
Bjorn Van den Broucke  
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Matteo Vettori  
Jian Xu

## **3Tex**

Alexander Bogdanovich  
Dmitry Mungalov

## **EADS Innovation Works**

Peter Middendorf  
Bjorn Van den Broucke

## **Uludag University**

Mehmet Karahan

## **Osaka University**

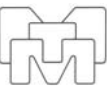
Tetsusei Kurashiki  
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Masaru Zako

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**EU:** TECABS; ITOOL; MOMENTUM; Marie Curie HPMT-CT-2000-00030

**Flanders:** STWW/000148; GBOU/020209

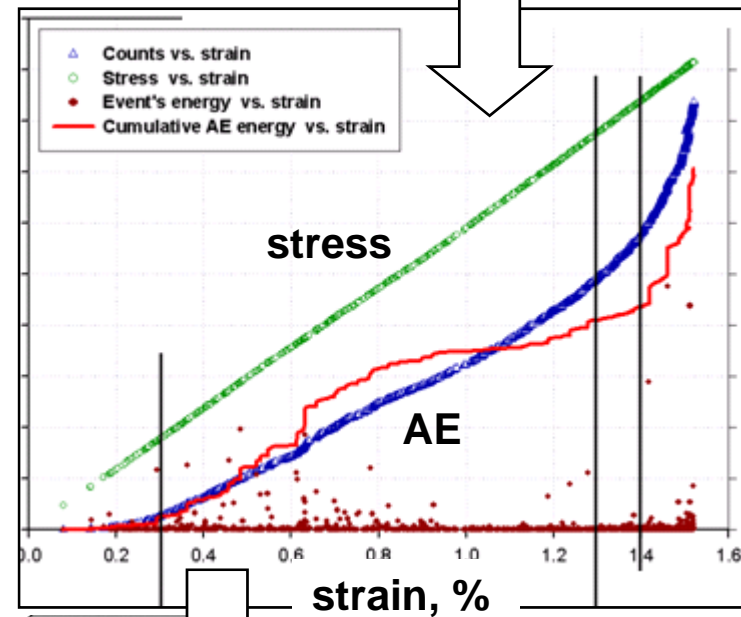
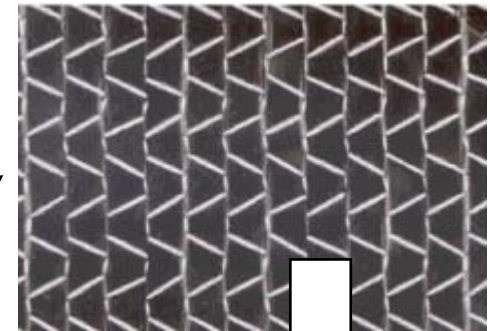
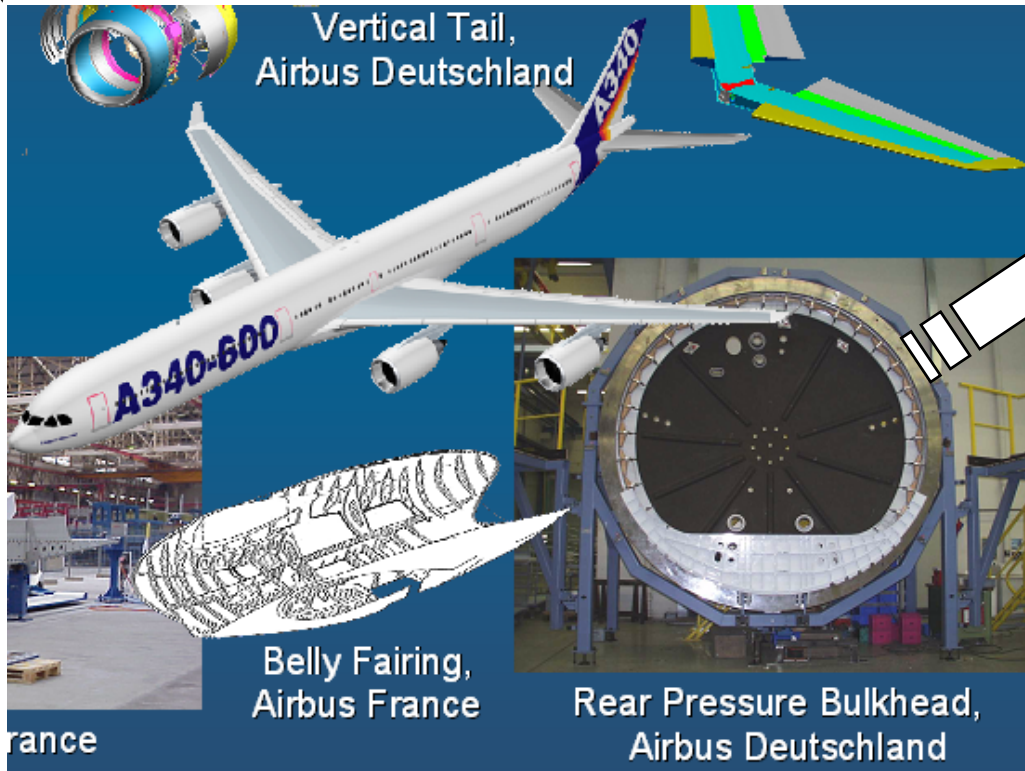
**K.U. Leuven:** GOA/98/05; OT/02/58



1. Introduction: What and Why and When and How and Where and Who?
2. Experimental: Road map for characterisation of damage in textile composites
3. Example: 2D and 3D woven glass/epoxy composites
4. Finite element analysis of damage: Predictions and numerical artifacts
5. Conclusions: Overview of damage studies with different textile architectures

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# Design strain and damage initiation threshold

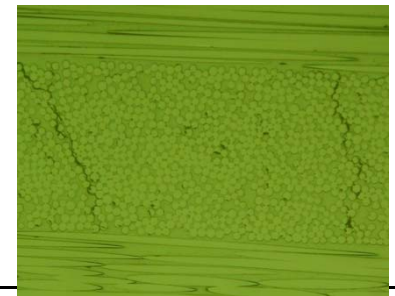
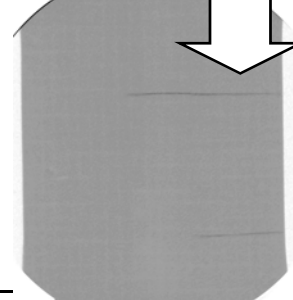


No stiffness reduction up to failure

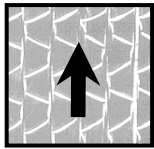
Design strain: 0.3 ... 0.4%

Ultimate strain / Design strain = 4...5

Corresponds to the damage initiation threshold

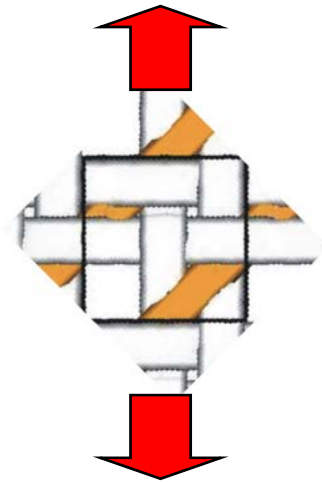
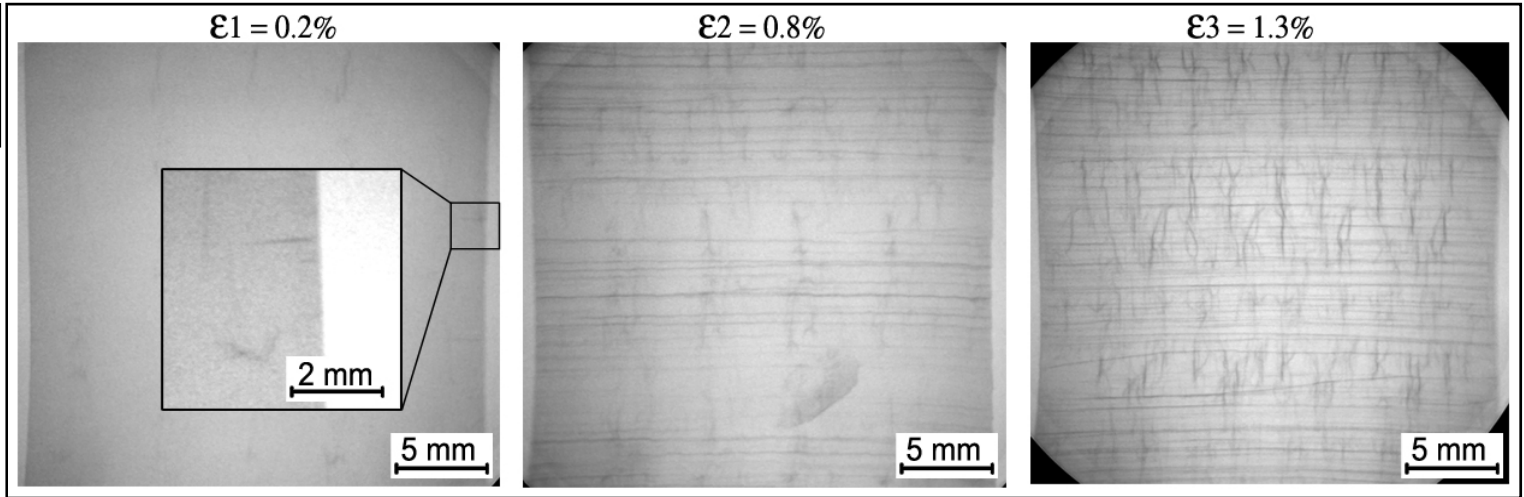


# Progressive damage: Patterns

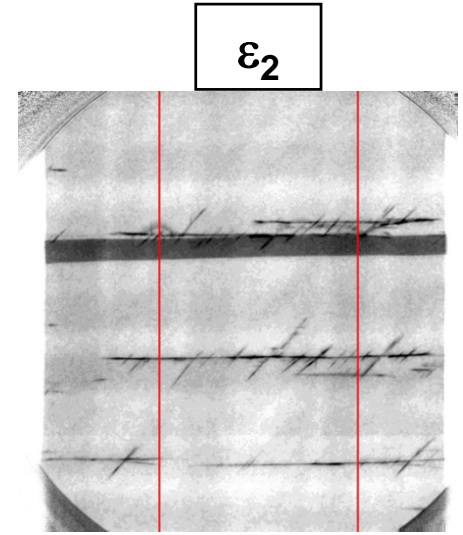
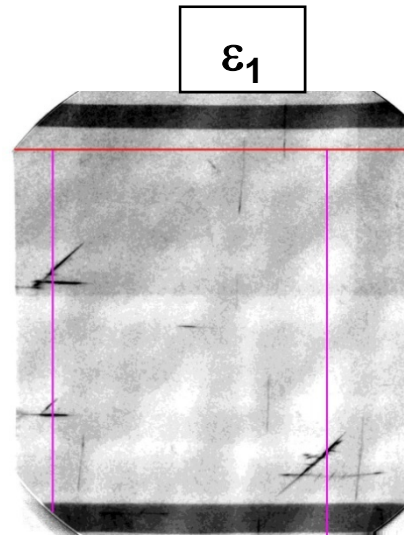


MD

Carbon/  
epoxy  
NCF

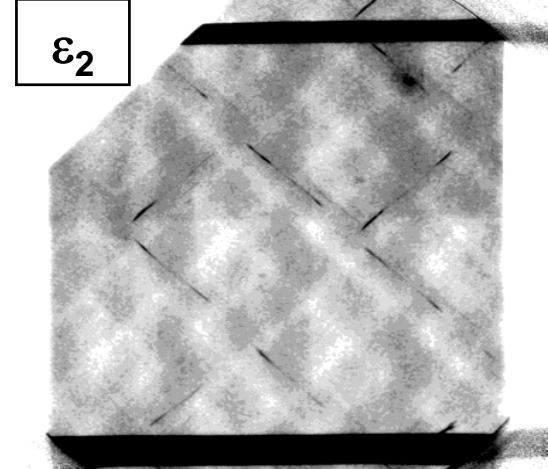
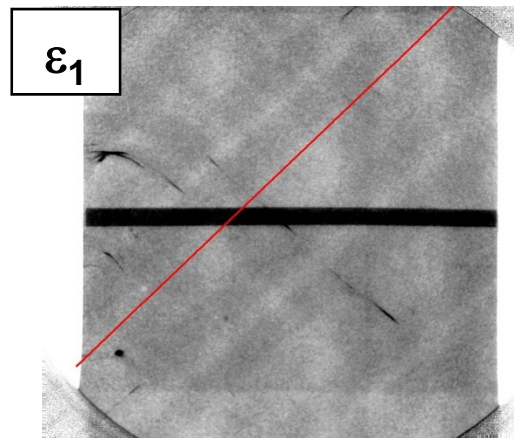
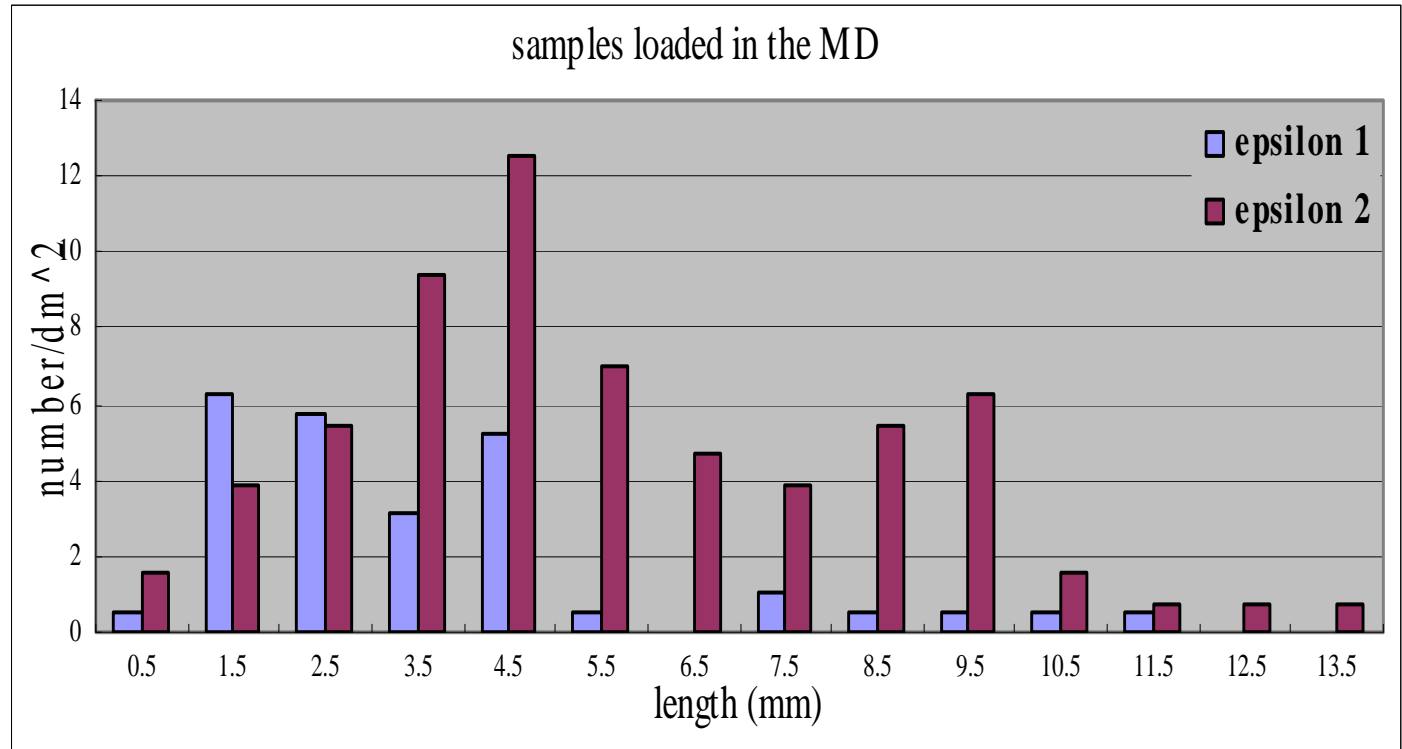


Carbon/ epoxy  
3-axial braid





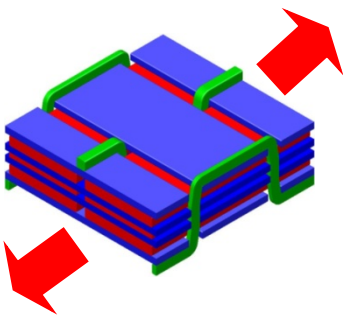
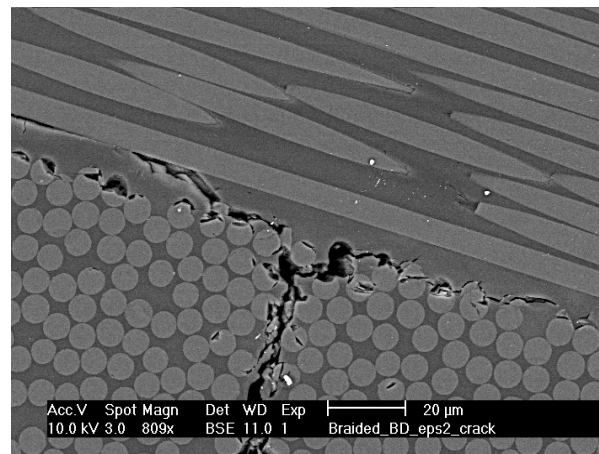
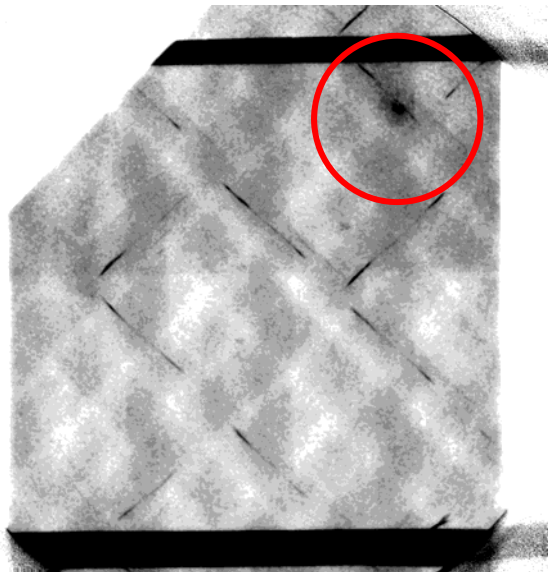
Carbon/ epoxy  
3-axial braid



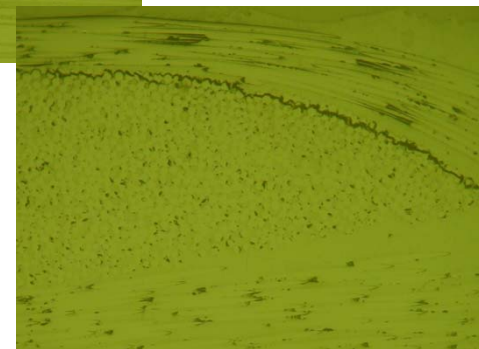
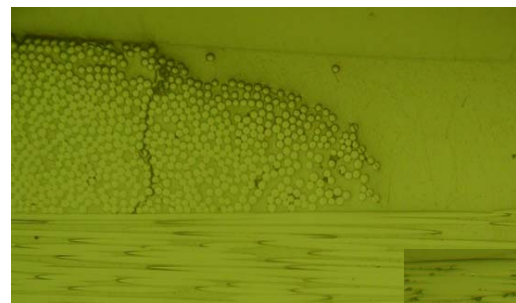
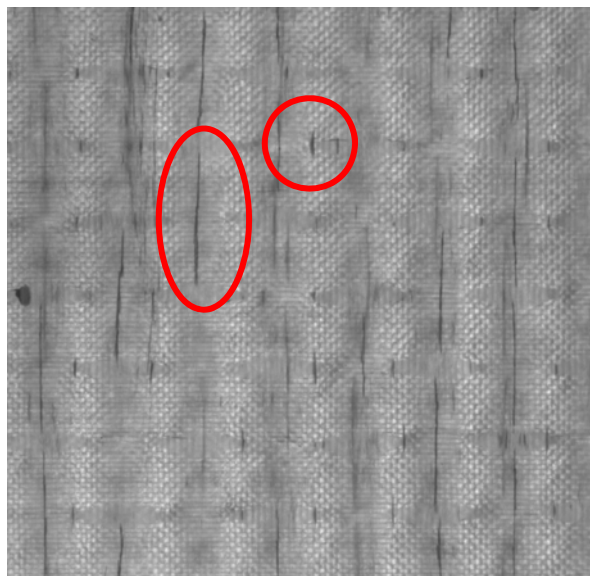
# Transversal cracks and bundle-boundary cracks



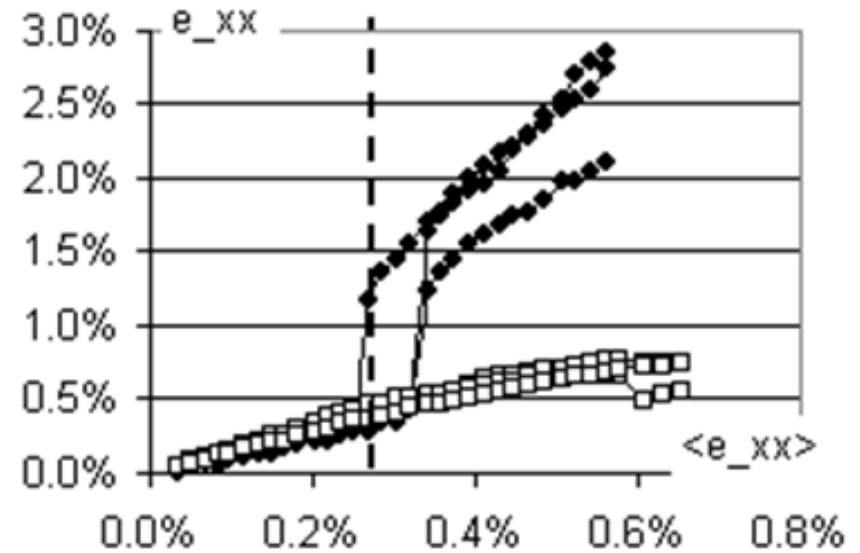
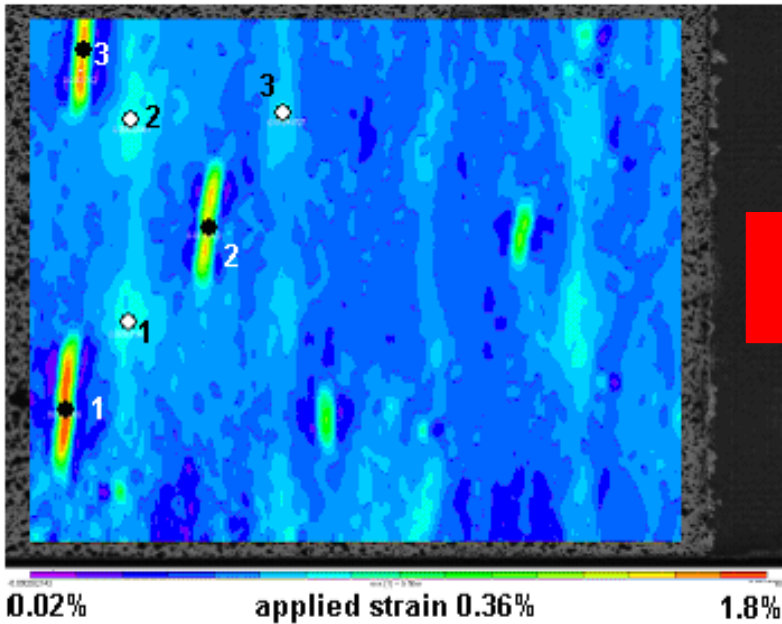
Carbon/ epoxy  
3-axial braid



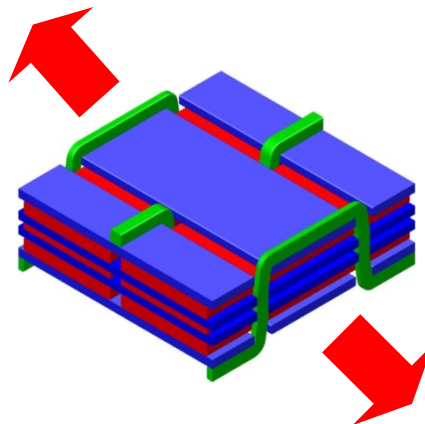
Glass-epoxy  
3D woven

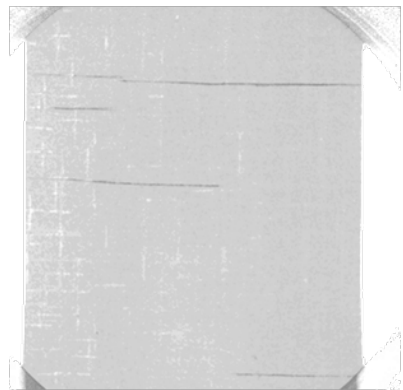
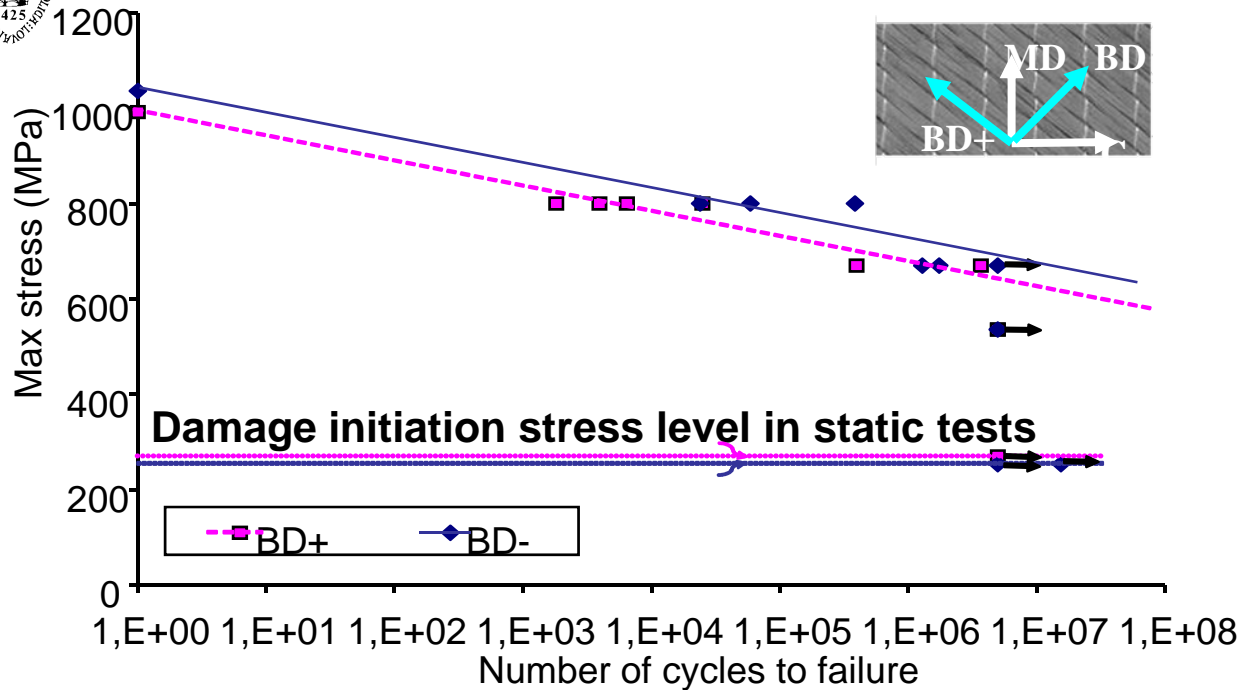






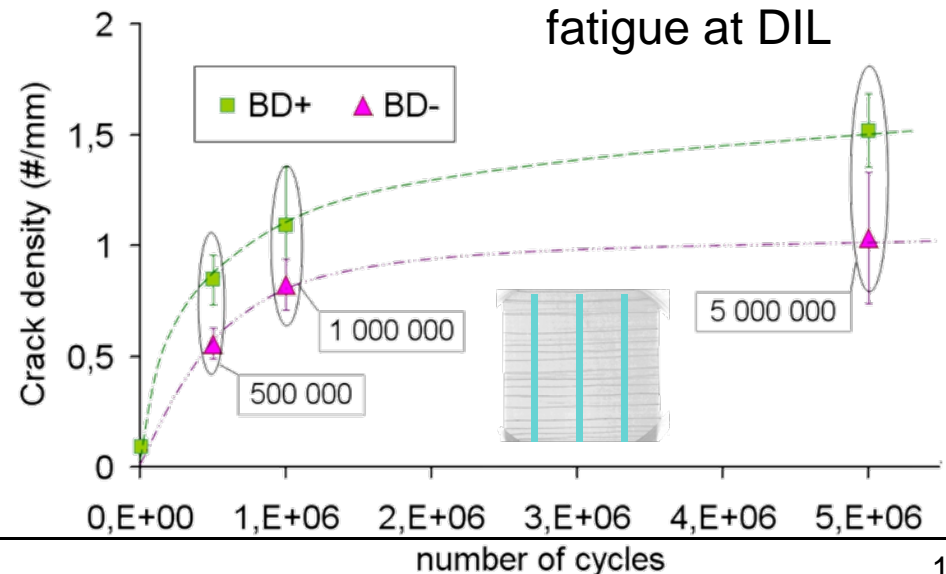
Glass-epoxy  
3D woven





5x10<sup>3</sup> cycles

5x10<sup>5</sup> cycles



- Damage induced by processing: Thermal and cure stresses
- Damage initiation (“first ply failure”, but localised)

Transversal damage inside fibre bundles

Boundaries of the bundles

- Damage propagation and associated reduction of the material stiffness

Grow and stoppage of the cracks

Multiplication of the cracks

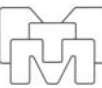
Correlations with the reinforcement structure

Fibre fracture

- Correlations quasi-static – fatigue



**"I have six honest serving men (they taught me all I knew).  
Their names are..."**



**...What** is happening to the material stiffness as damage is progressing?

*Non-linear tensile diagram*

**...Why** has damage been initiated?

*The cause of the first crack(s)*

**...When** has damage been initiated?

*Damage initiation threshold*

**...How** does damage progress?

*Propagation and multiplication of cracks and local debondings*

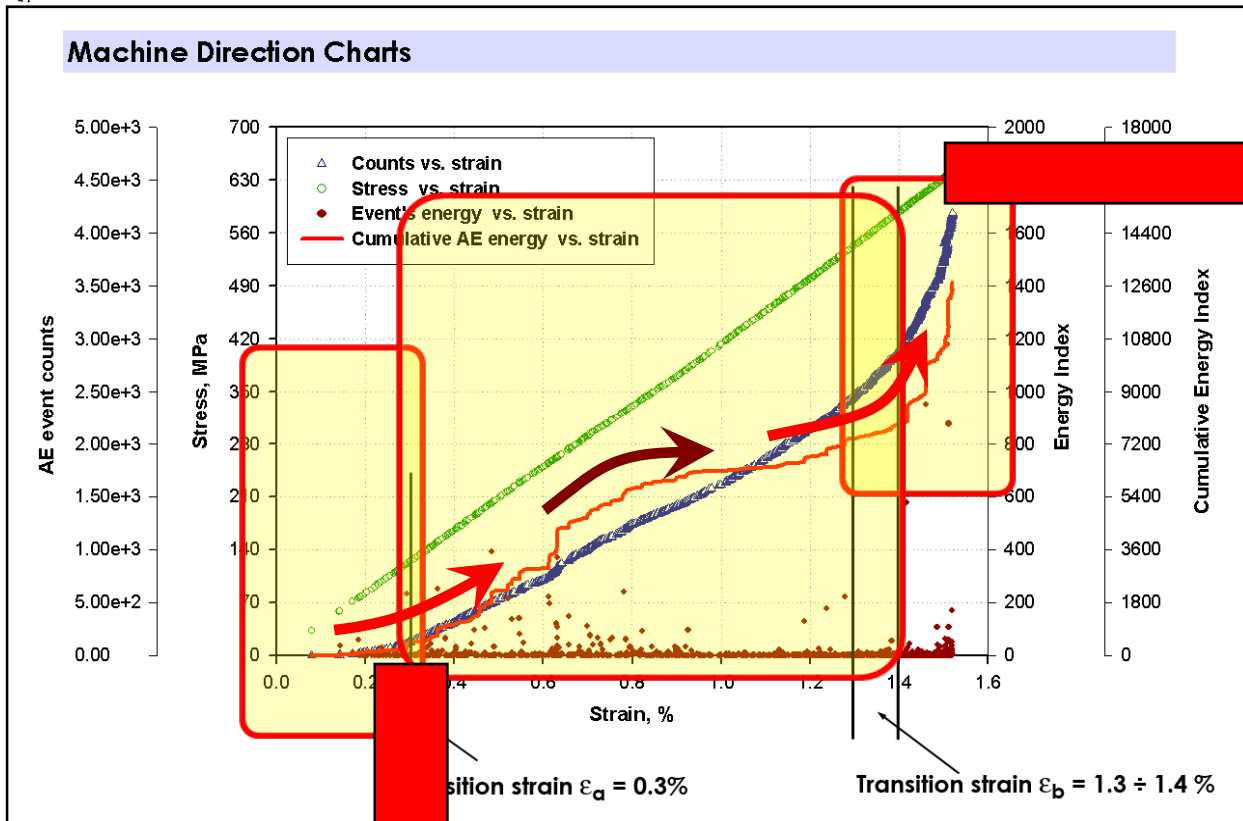
**...Where** are the damage locations inside the reinforcement unit cell?

*Inside the impregnated yarns? On their boundaries? In matrix pockets?*

**...Who** (which damage modes) are in evidence?

*Transversal? Shear? Debondings? Delaminations? Splitting?..*

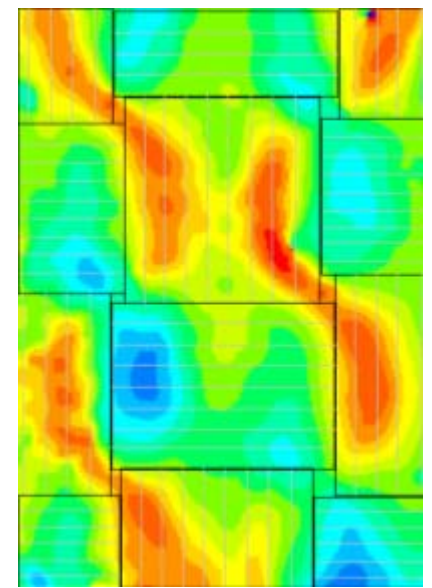
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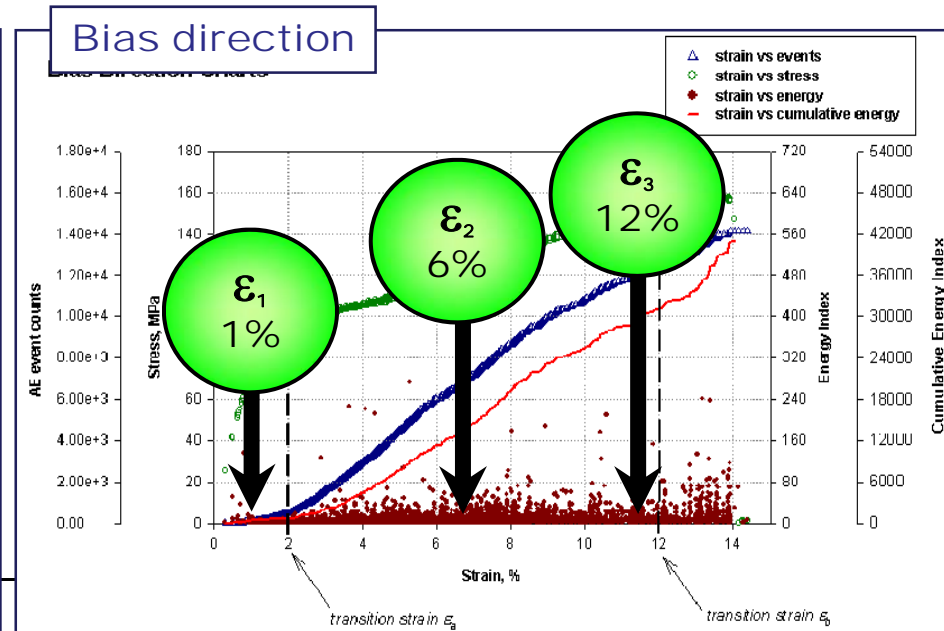
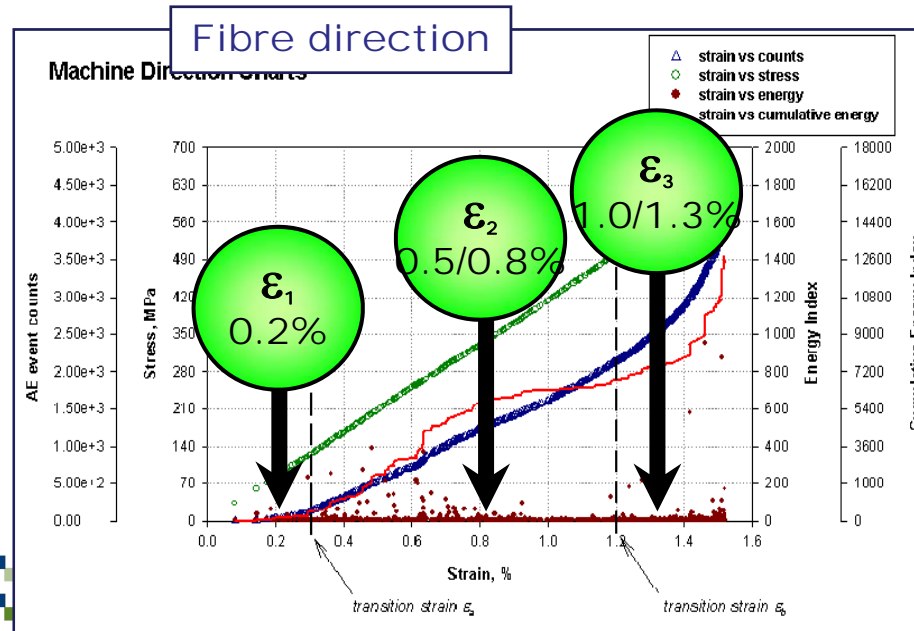
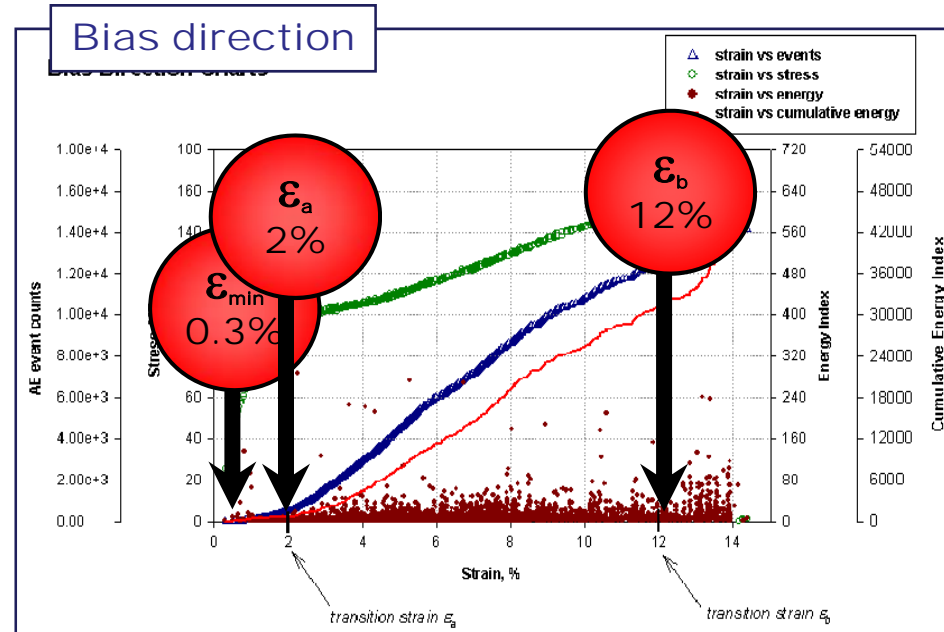
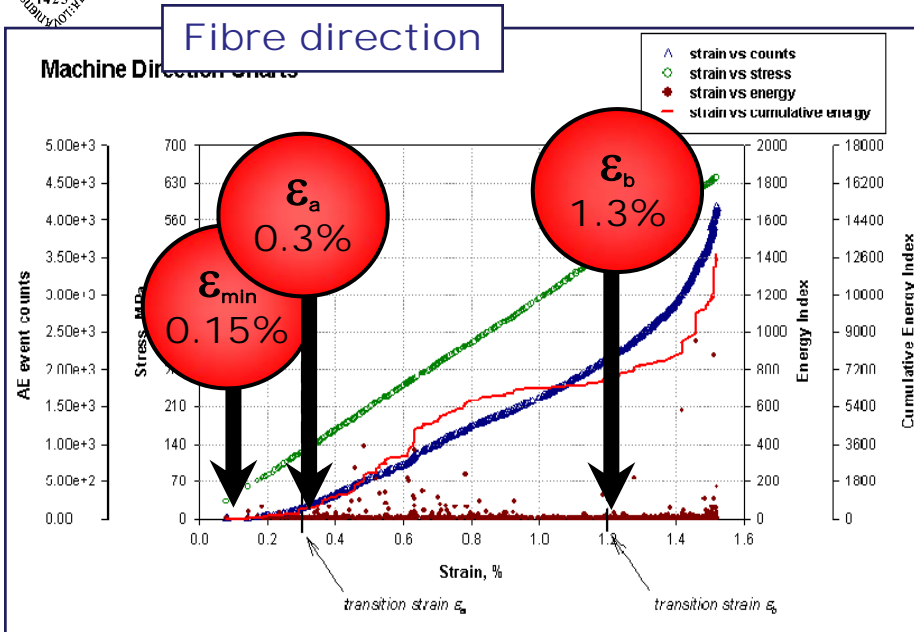


**Tension diagram**

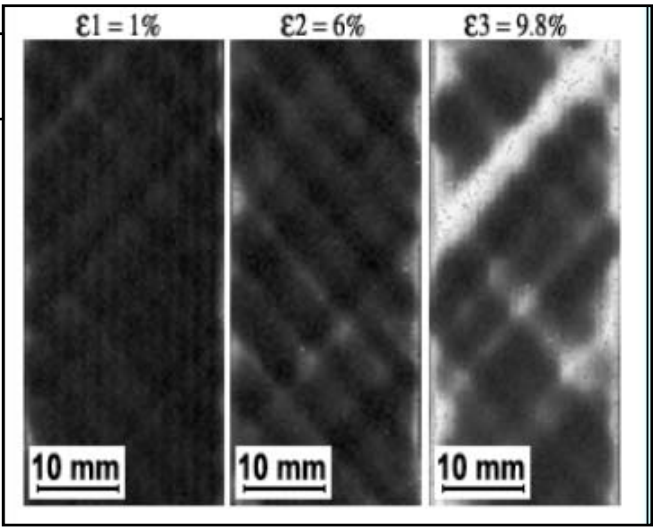
**AE: Damage initiation threshold**

**Strain maps**





**C-scan**

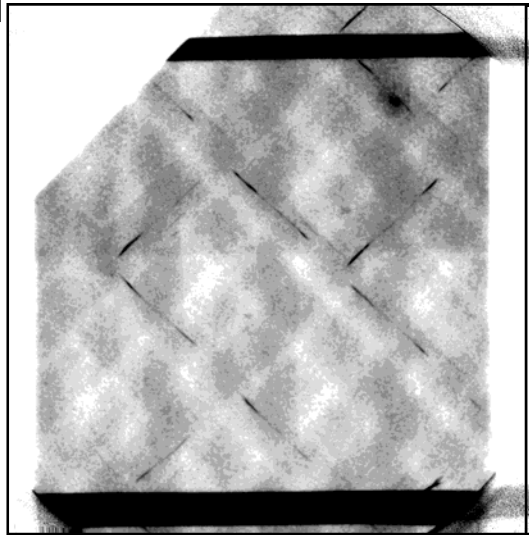


**Dynamics of extent of damage**

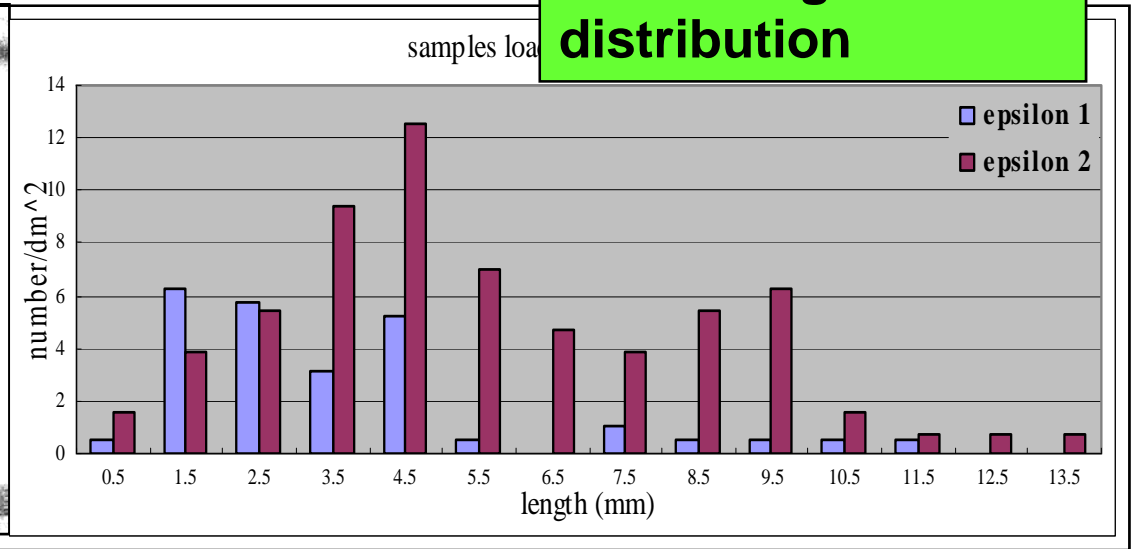
**Damage periodicity**

**Cracks placement and orientation**

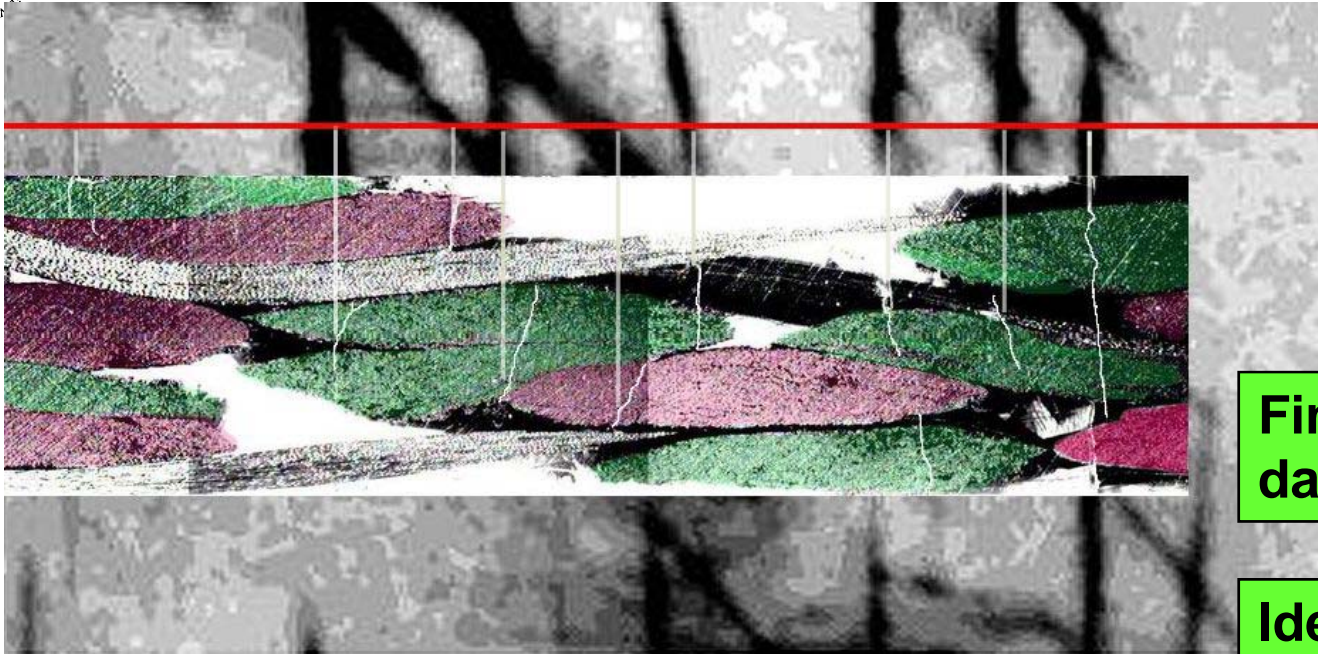
**X-ray**



**Crack length distribution**

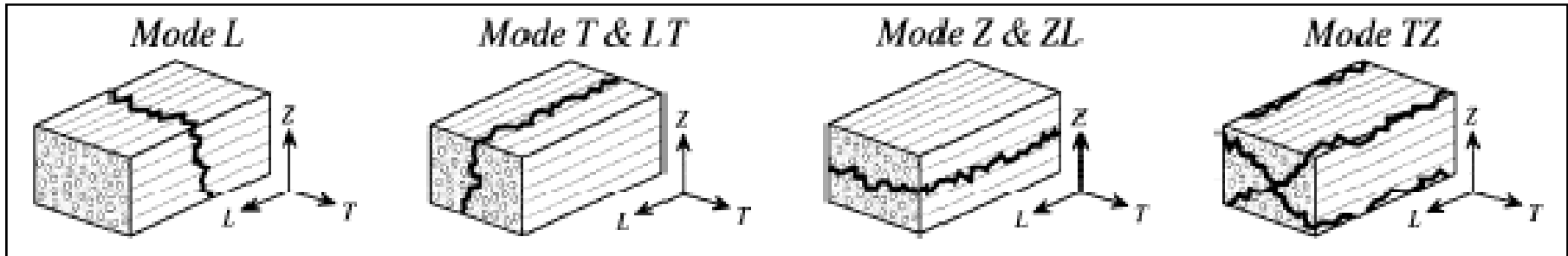


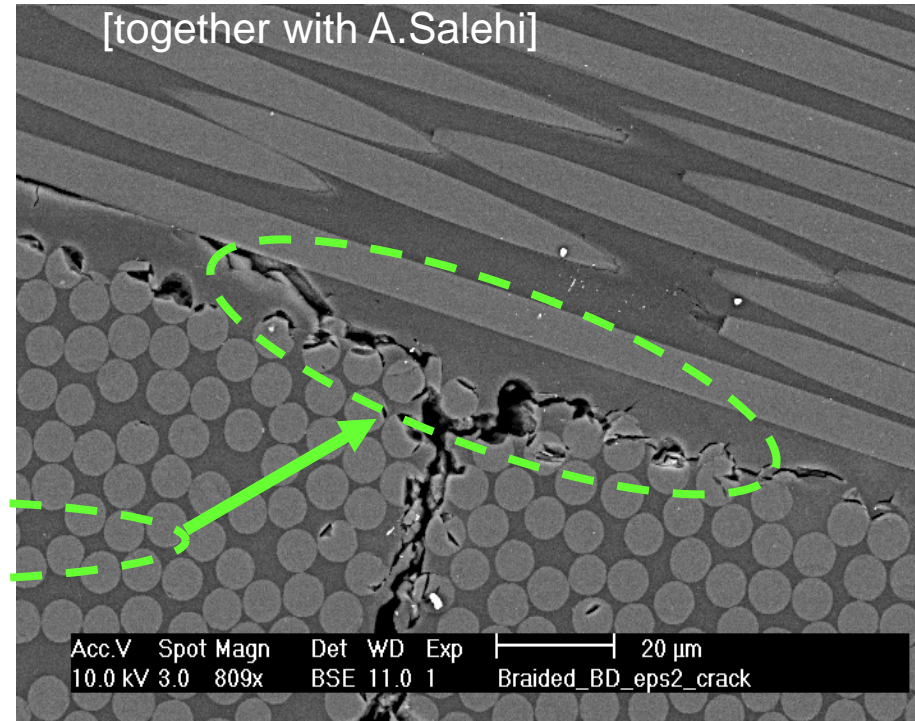
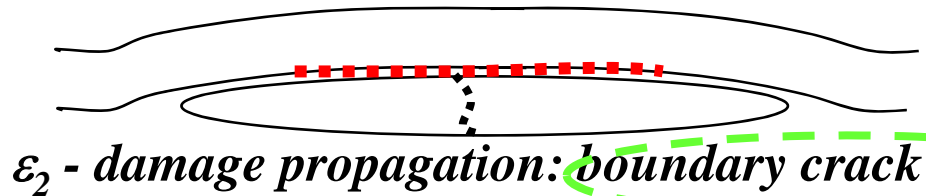
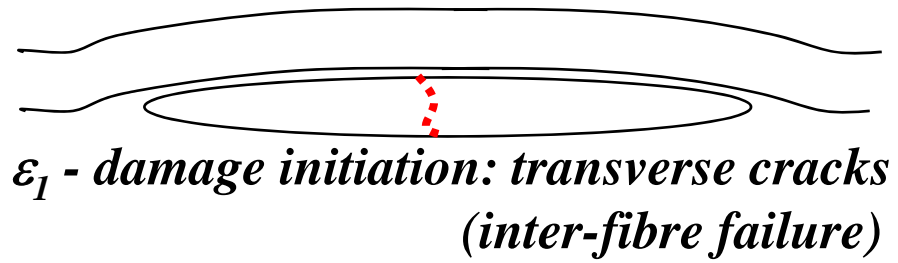




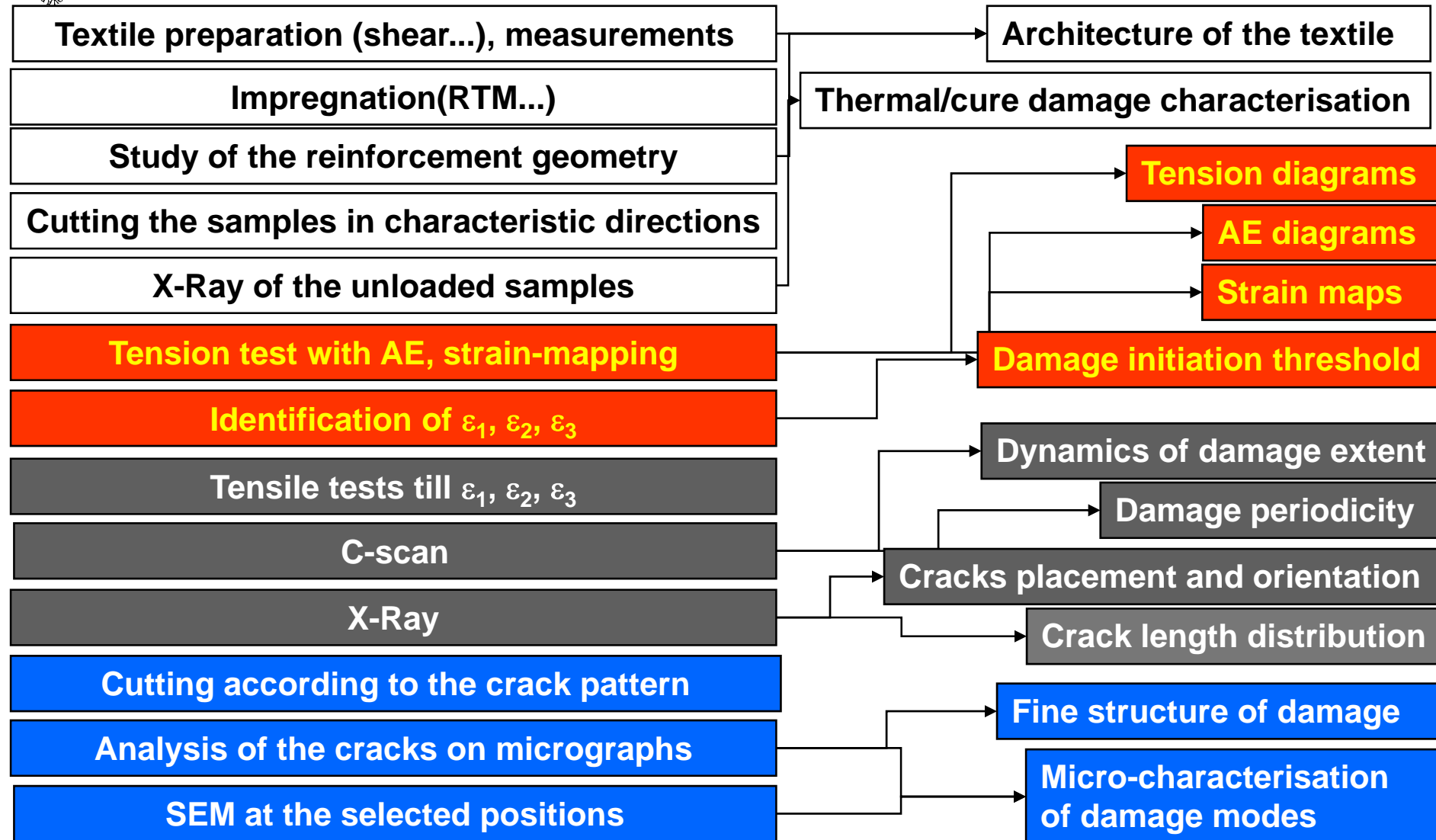
Fine structure of damage

Identification of damage modes





**Micro-characterisation of damage modes**



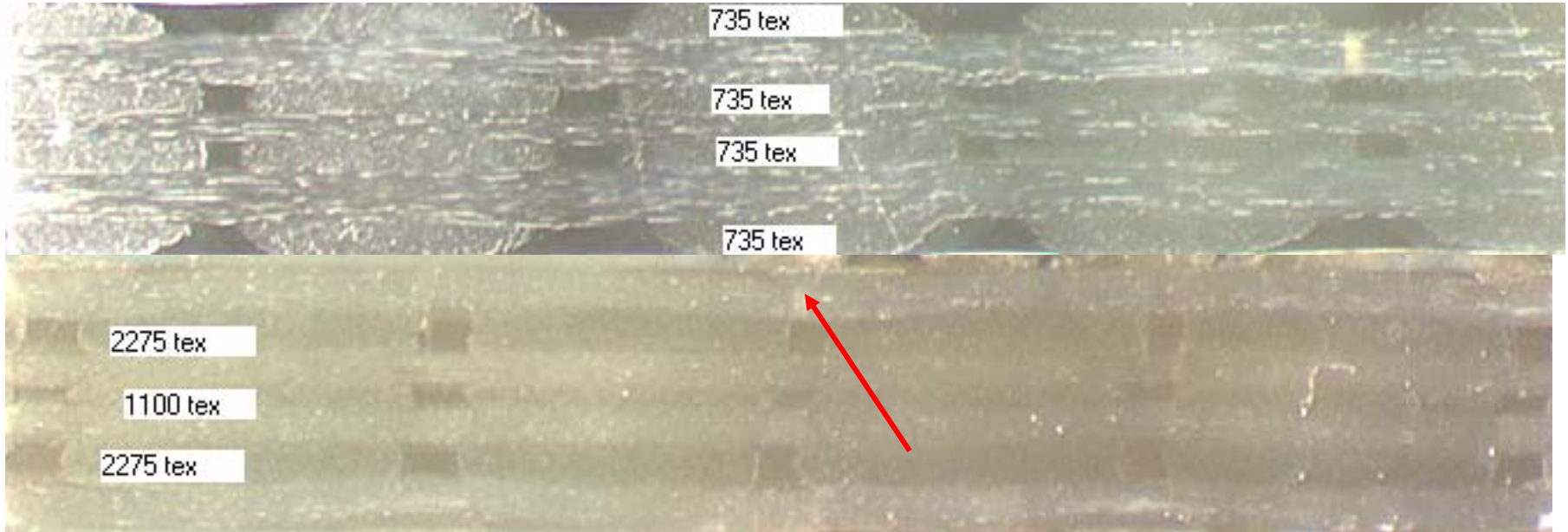
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collaborative research with 3Tex: A.E. Bogdanovich, D. Mungalov



# Internal structure of 3D and plain weave composites

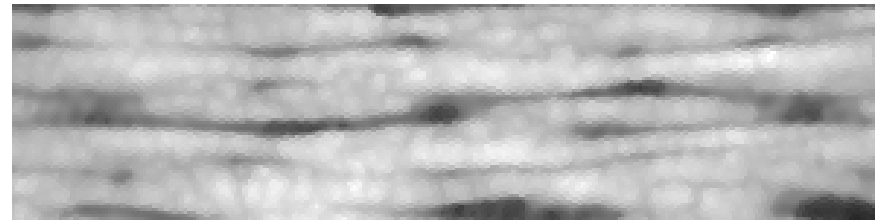
96 oz 3WEAVE® E-Glass 2022 Silane Sized  
Part No: P3W-GE044



- Note:
1. Slight crimp of the fill caused by compaction in VARTM
  2. Almost rectangular shape of the cross-sections

Plain weave laminate

Crimped warp/weft, nested plies



3D – GE044

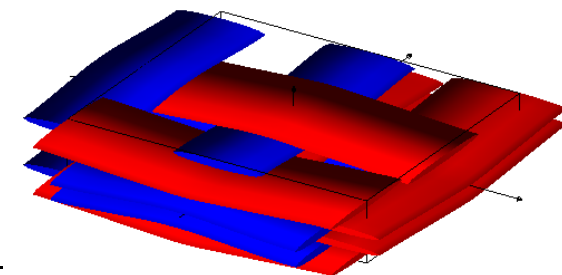
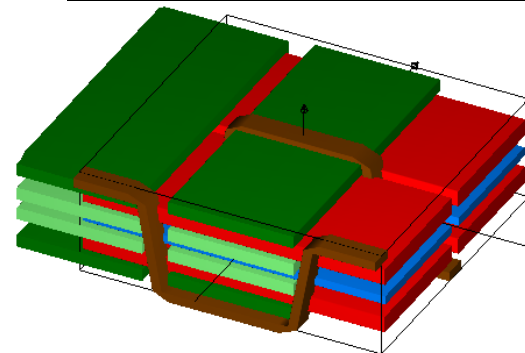
3WEAVE®

Plain weave

4 plies: 0°/90°/90°/0°

<b>Fabric and composite plate</b>	1 ply
<b>Areal density, g/m<sup>2</sup></b>	<b>3255</b>
<b>Thickness, mm</b>	<b>2.6</b>
Ends (straight) per cm per layer	2.76
Picks per cm	2.64
Z-yarns per cm	2.76
<b>VF, %</b>	<b>48.9</b>
<b>Yarns</b>	<b>tex</b>
<i>Warp</i>	
layer 1,3	2275
layer 2	1100
Z-yarns	276
<i>Fill (double yarns)</i>	
layer 1,4	1470
layer 2,3	1470

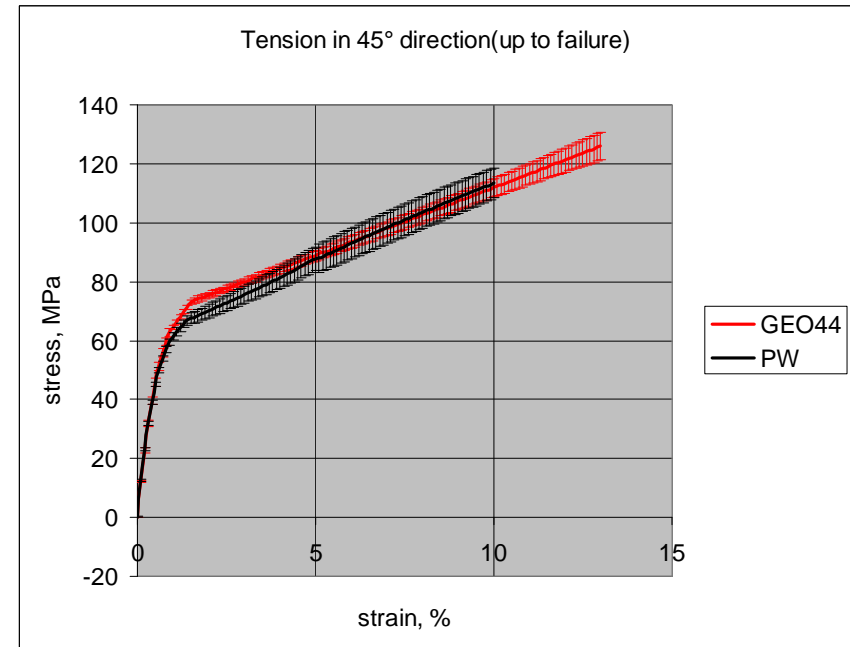
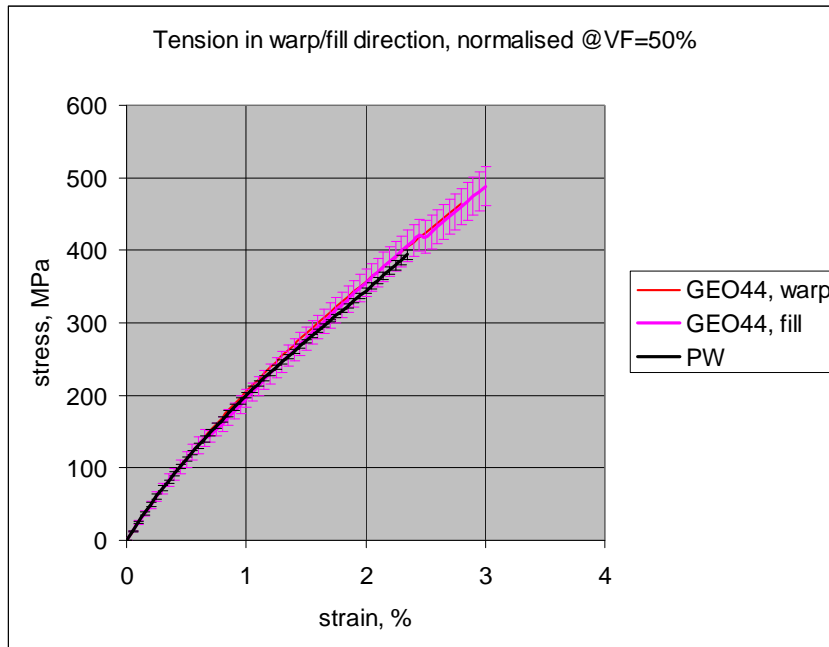
<b>Fabric and composite plate</b>	4 ply
<b>Areal density, g/m<sup>2</sup></b>	<b>3260</b>
<b>Thickness, mm</b>	<b>2.45</b>
Ends per cm	5.08
Picks per cm	6.19
<b>VF, %</b>	<b>52.4</b>
<b>Yarns</b>	<b>tex</b>
<i>Warp and weft</i>	2275



Warp : Fill : Z = 49% : 48% : 2%

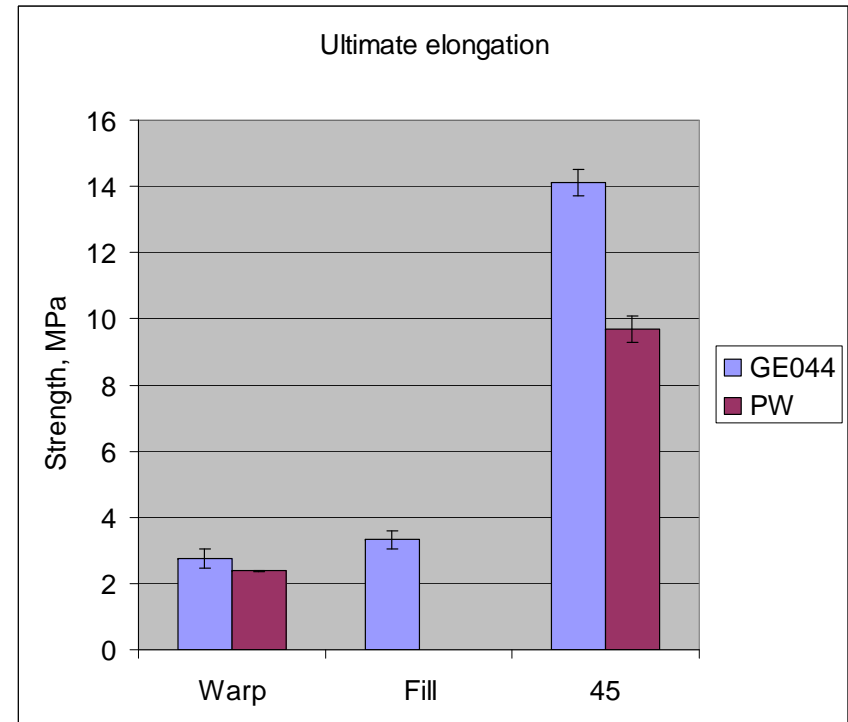
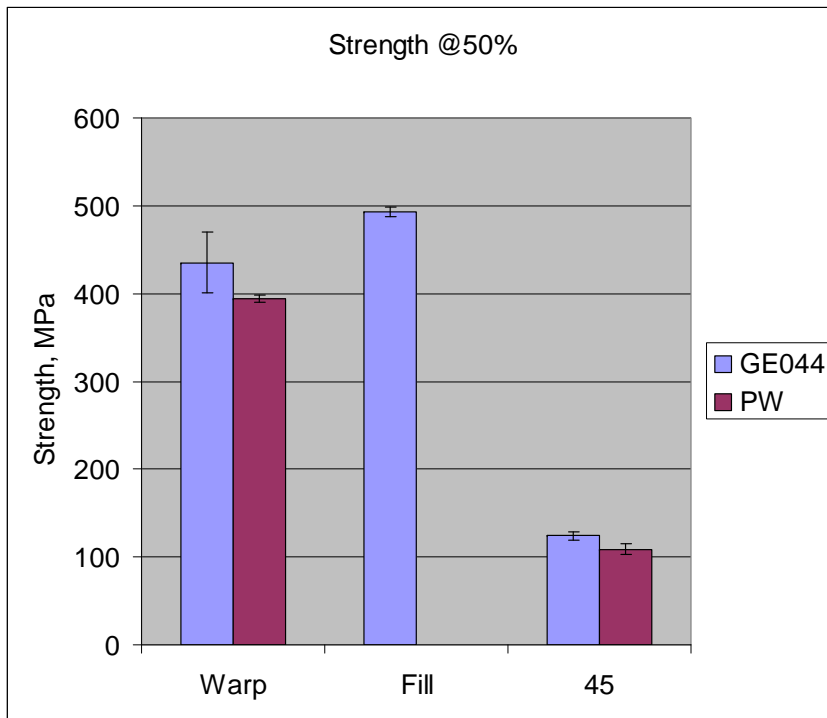
# Elastic constants and tension diagrams

	VF, %		E, MPa		Poisson		sigU, MPa		epsU, %		eps1, %		eps2, %	
GE044	49.3	Warp	24297	1207	0.141	0.071	429	34	2.74	0.29	0.43	0.04	0.54	0.04
		Fill	25112	2340	0.126	0.093	486	5	3.33	0.27	0.37	0.06	0.59	0.04
		45	12913	485	0.502	0.21	124	5	14.1	0.4	0.63	0.07	0.78	0.07
PW	52.4	Warp	26005	1558	0.264	0.148	413	4	2.38	0.02	0.26	0.04	0.43	0.06
		45	12233	444	0.61	0.148	109	6	9.7	0.4	1.23	0.35	2.33	0.93



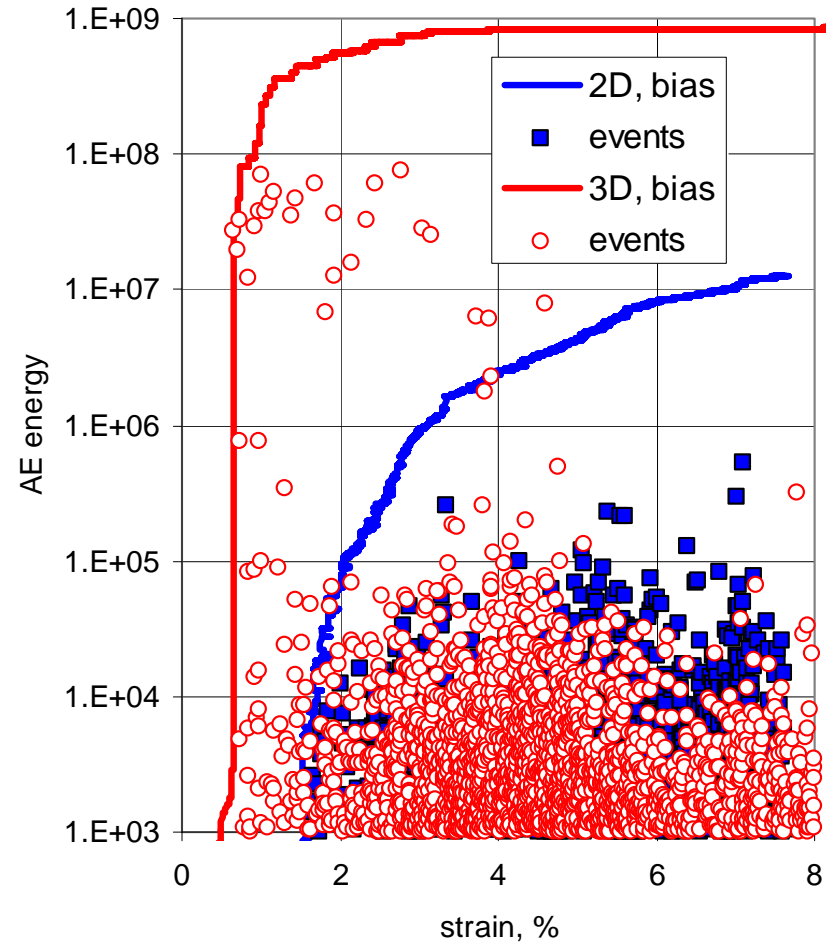
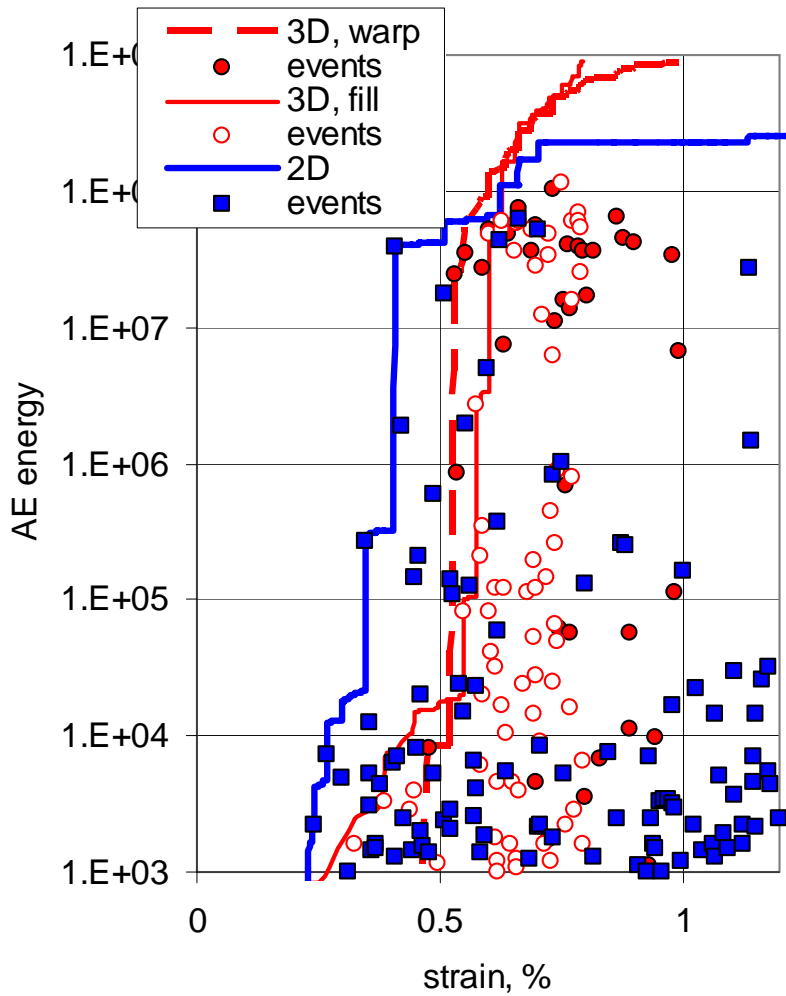
- No difference in Young moduli
- Decreased Poisson for the 3D fabric (inside the scatter?)

	VF, %		E, MPa		Poisson		sigU, MPa		epsU, %		eps1, %		eps2, %	
GE044	49.3	Warp	24297	1207	0.141	0.071	429	34	2.74	0.29	0.43	0.04	0.54	0.04
		Fill	25112	2340	0.126	0.093	486	5	3.33	0.27	0.37	0.06	0.59	0.04
	45	12913	485	0.502	0.21	124	5	14.1	0.4	0.63	0.07	0.78	0.07	
PW	52.4	Warp	26005	1558	0.264	0.148	413	4	2.38	0.02	0.26	0.04	0.43	0.06
		45	12233	444	0.61	0.148	109	6	9.7	0.4	1.23	0.35	2.33	0.93



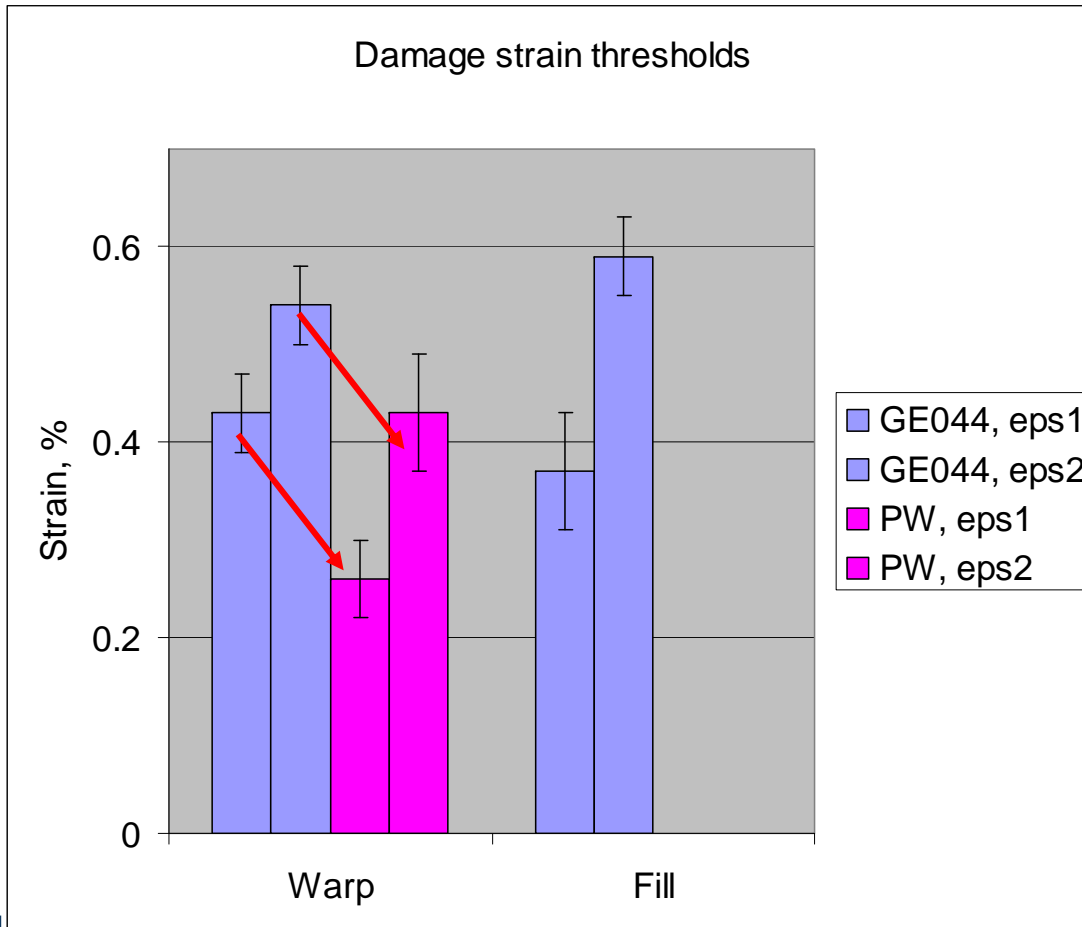
3D composite: higher strength (+10%), higher elongation





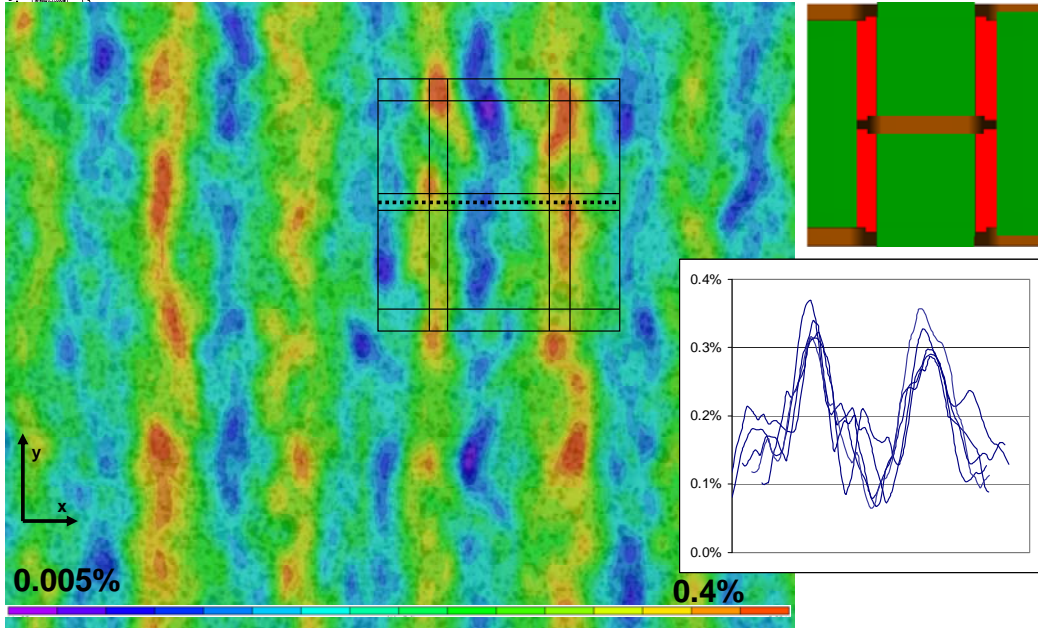
# Damage thresholds

	VF, %		E, MPa		Poisson		sigU, MPa		epsU, %		eps1, %		eps2, %	
GE044	49.3	Warp	24297	1207	0.141	0.071	429	34	2.74	0.29	0.43	0.04	0.54	0.04
		Fill	25112	2340	0.126	0.093	486	5	3.33	0.27	0.37	0.06	0.59	0.04
		45	12913	485	0.502	0.21	124	5	14.1	0.4	0.63	0.07	0.78	0.07
PW	52.4	Warp	26005	1558	0.264	0.148	413	4	2.38	0.02	0.26	0.04	0.43	0.06
		45	12233	444	0.61	0.148	109	6	9.7	0.4	1.23	0.35	2.33	0.93

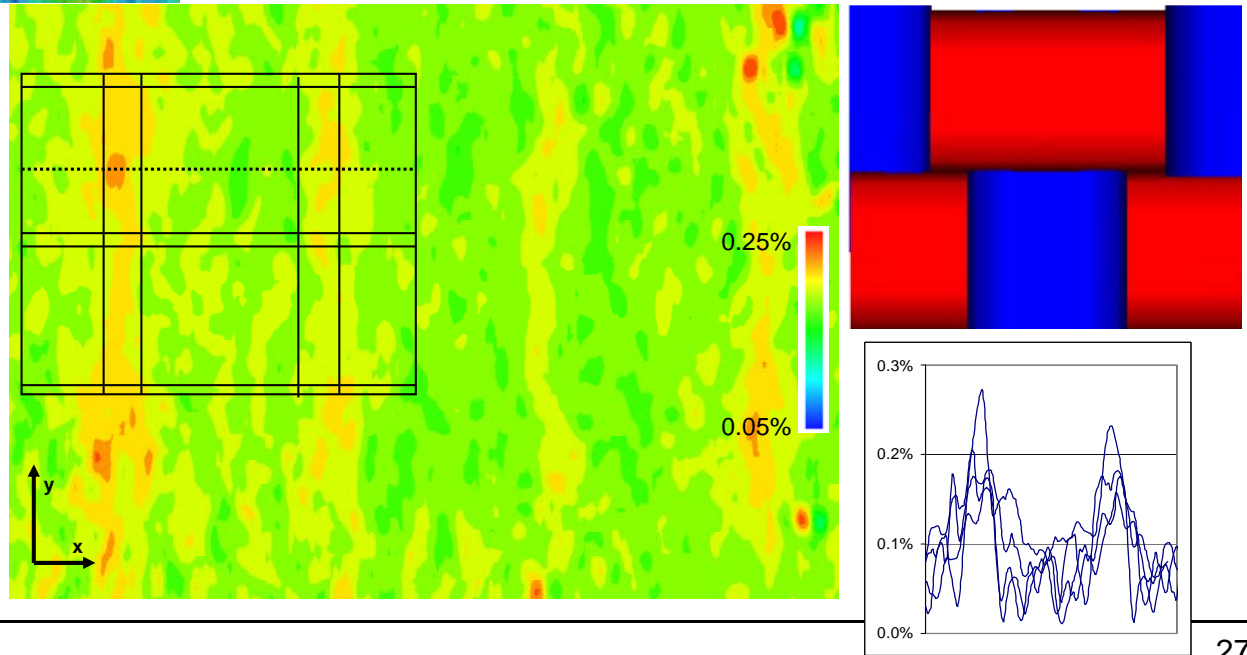


## 3D composite:

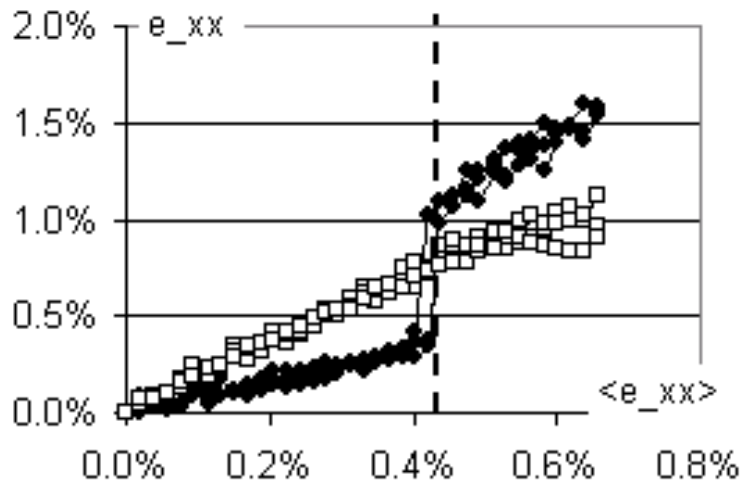
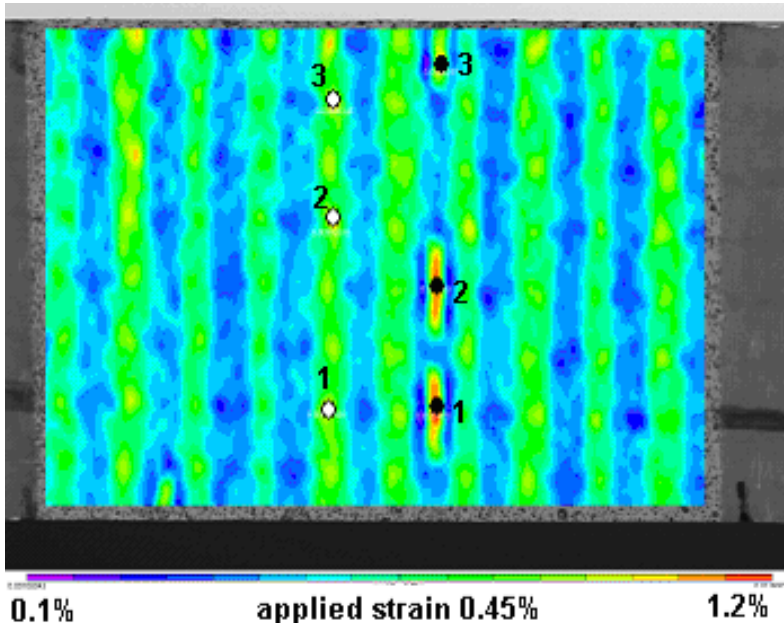
- increase of damage initiation thresholds by 0.2% strain for loading in fibre direction
- advantage in fatigue life stress limit can be expected
- lower damage thresholds for loading in bias direction



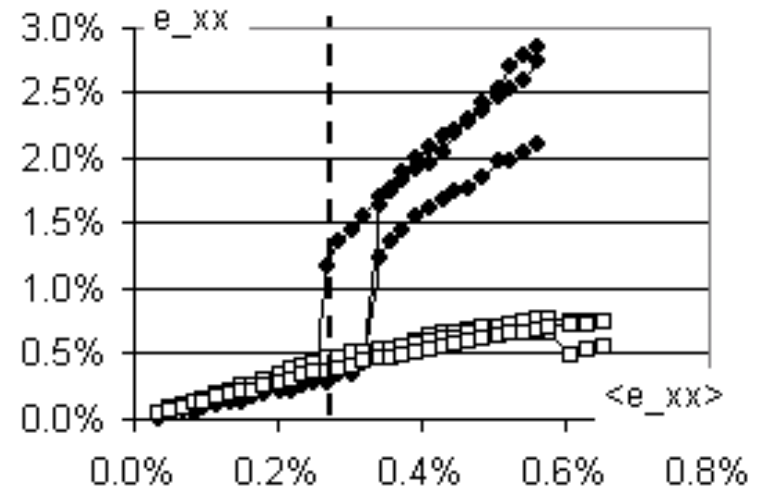
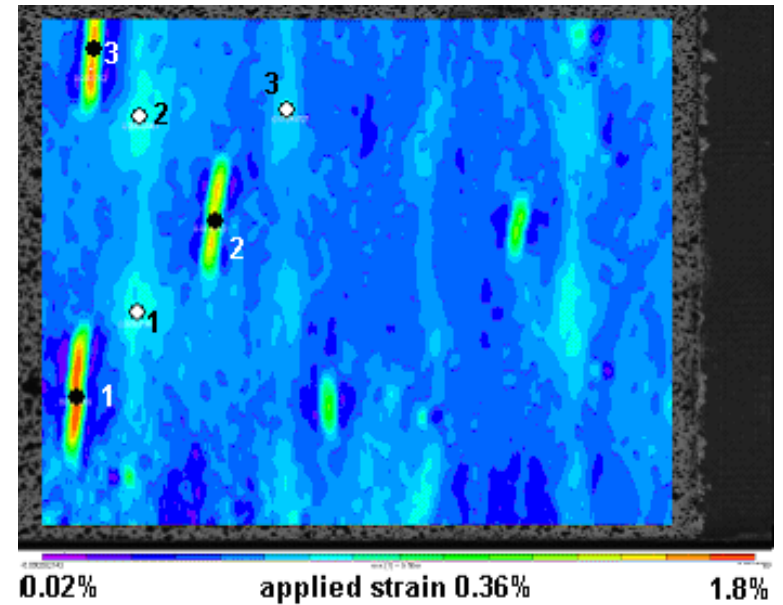
plain  
weave



GE044



plain weave

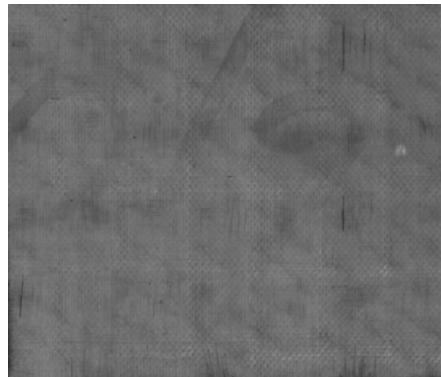


# Damage development: Loading in WARP direction

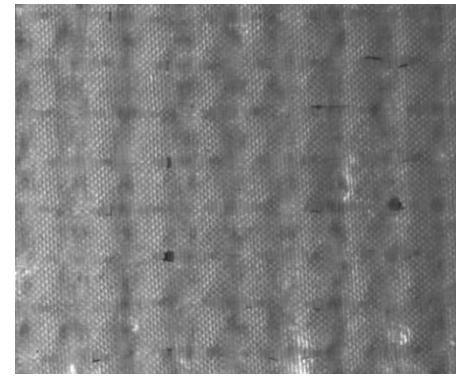
plain weave

GE044

0.30%

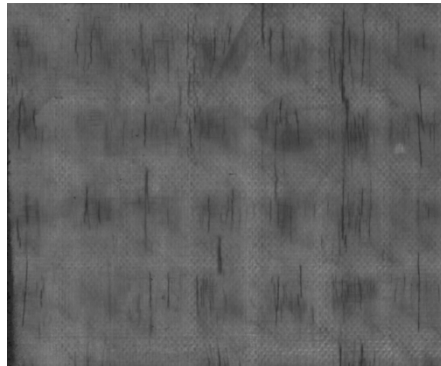


onset of transverse cracks in fill

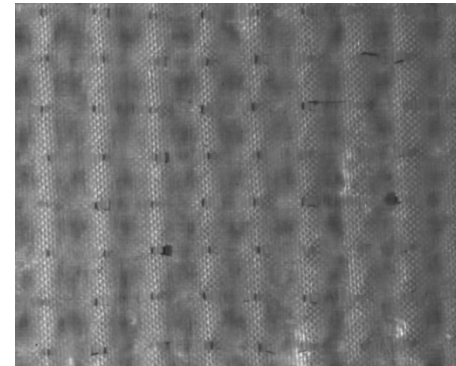


onset of bundle-boundary cracks on Z-yarns

0.50%

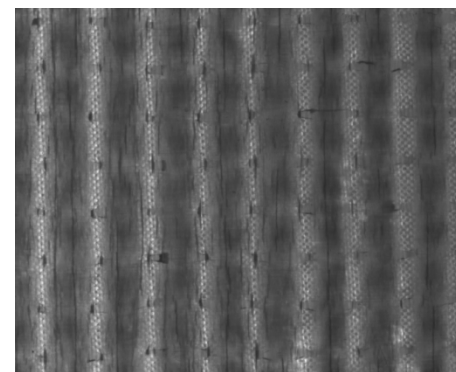
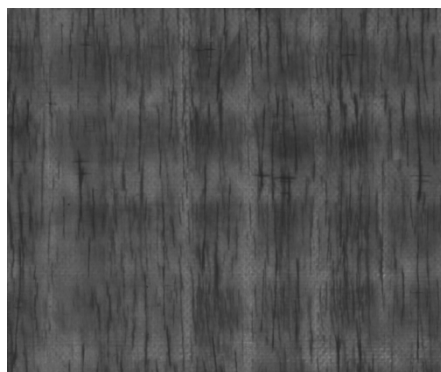


intensive transverse cracks in fill and intra-yarn cracks parallel to the yarn surface



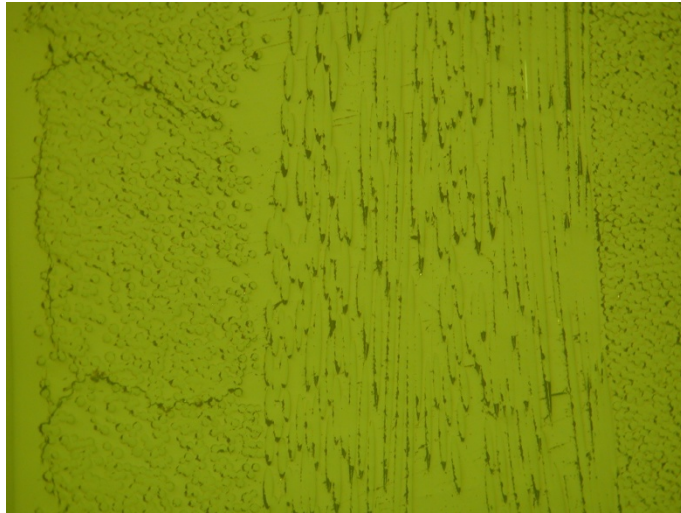
onset of transverse cracks in fill

1.0%



transverse cracks and bundle-boundary cracks in fill and Z-yarns

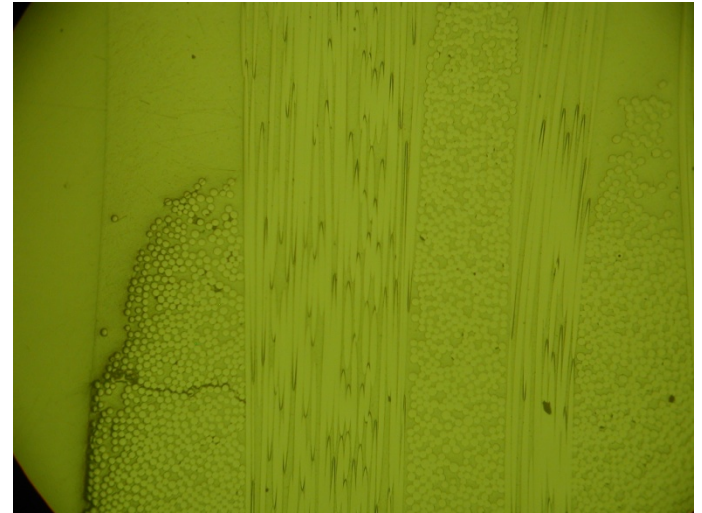
transverse crack in fill



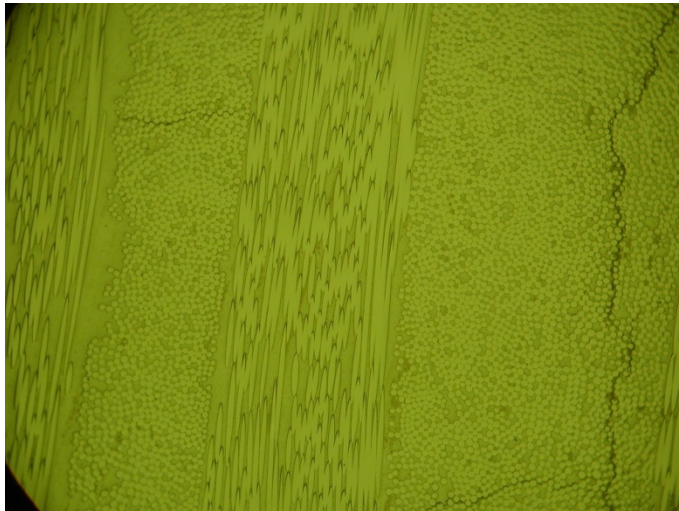
plain  
weave

GE044

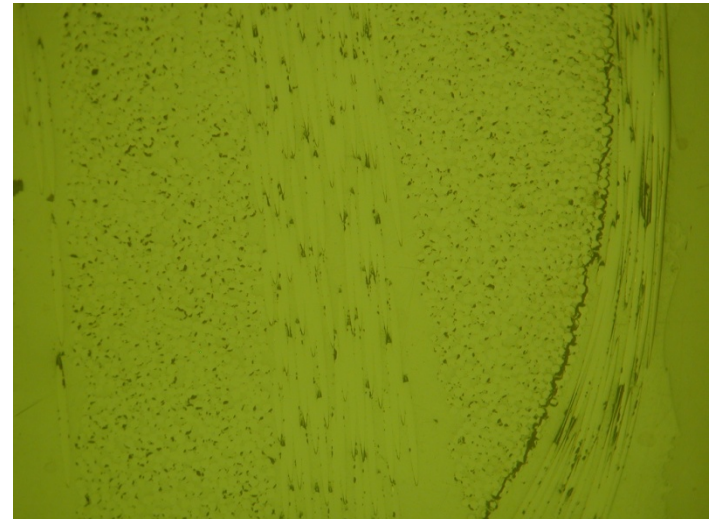
transverse crack in fill



intra-yarn crack parallel to yarn surface



bundle-boundary crack, Z-yarn



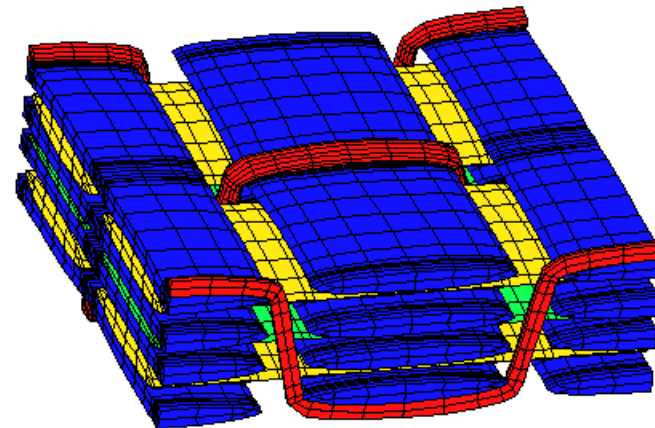
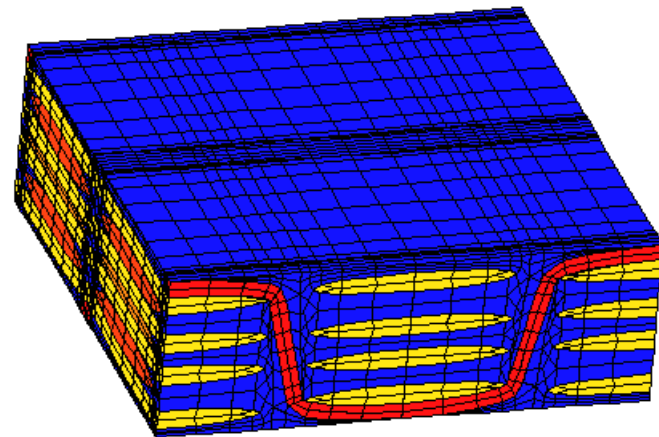
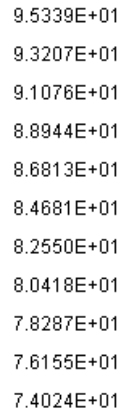
1. Introduction: What and Why and When and How and Where and Who?
2. Experimental: Road map for characterisation of damage in textile composites
3. Example: 2D and 3D woven glass/epoxy composites
4. Finite element analysis of damage: Predictions and numerical artifacts
  - Example: 3D woven glass/epoxy composite, loading in WARP direction
5. Conclusion: Overview of damage studies with different textile architectures

collaborations:

- 3Tex: A.E. Bogdanovich, D. Mungalov
- Osaka University: K. Hamada, T. Kurashiki, M. Zako



VolumeFraction



Geometric modeller	WiseTex
Geometry corrector of yarn interpenetration	MeshTex
Meshing	
Material properties	
Boundary conditions	SACOM
FE solver, post-processor	
Homogenisation	
Damage	

UD	MPa	Matrix	MPa
L, tensile	1725	Tension	76
L, compr.	620	Compr.	112
T, tensile	40	Shear	86
T, compr.	140		
LT	70		
TZ	70		



## Damage initiation: Hoffmann

$$F = C_1(\sigma_T - \sigma_Z)^2 + C_2(\sigma_Z - \sigma_L)^2 + C_3(\sigma_L - \sigma_T)^2 + C_4\sigma_L + C_5\sigma_T + C_6\sigma_Z + C_7\tau_{TZ}^2 + C_8\tau_{ZL}^2 + C_9\tau_{LT}^2$$

$$C_1 = \frac{1}{2} \left( \frac{1}{F_T^t F_T^c} + \frac{1}{F_Z^t F_Z^c} - \frac{1}{F_L^t F_L^c} \right)$$

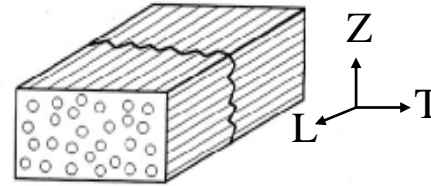
$$C_2 = \frac{1}{2} \left( \frac{1}{F_Z^t F_Z^c} + \frac{1}{F_L^t F_L^c} - \frac{1}{F_T^t F_T^c} \right)$$

$$C_3 = \frac{1}{2} \left( \frac{1}{F_L^t F_L^c} + \frac{1}{F_T^t F_T^c} - \frac{1}{F_Z^t F_Z^c} \right)$$

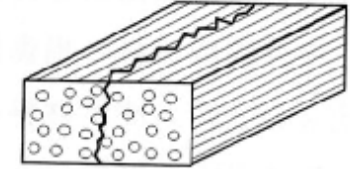
$$C_4 = \frac{1}{F_L^t} - \frac{1}{F_L^c}, C_5 = \frac{1}{F_T^t} - \frac{1}{F_T^c}, C_6 = \frac{1}{F_Z^t} - \frac{1}{F_Z^c}$$

$$C_7 = \left( \frac{1}{F_{TZ}^s} \right)^2, C_8 = \left( \frac{1}{F_{ZL}^s} \right)^2, C_9 = \left( \frac{1}{F_{LT}^s} \right)^2$$

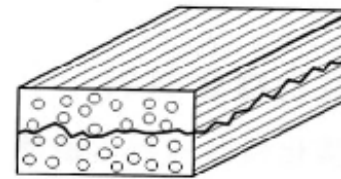
## Definition of the damage mode



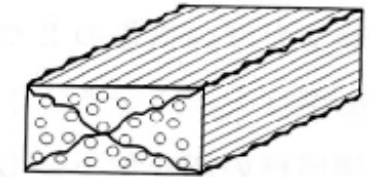
(a) Mode L



(b) Mode T&LT



(c) Mode Z&ZL



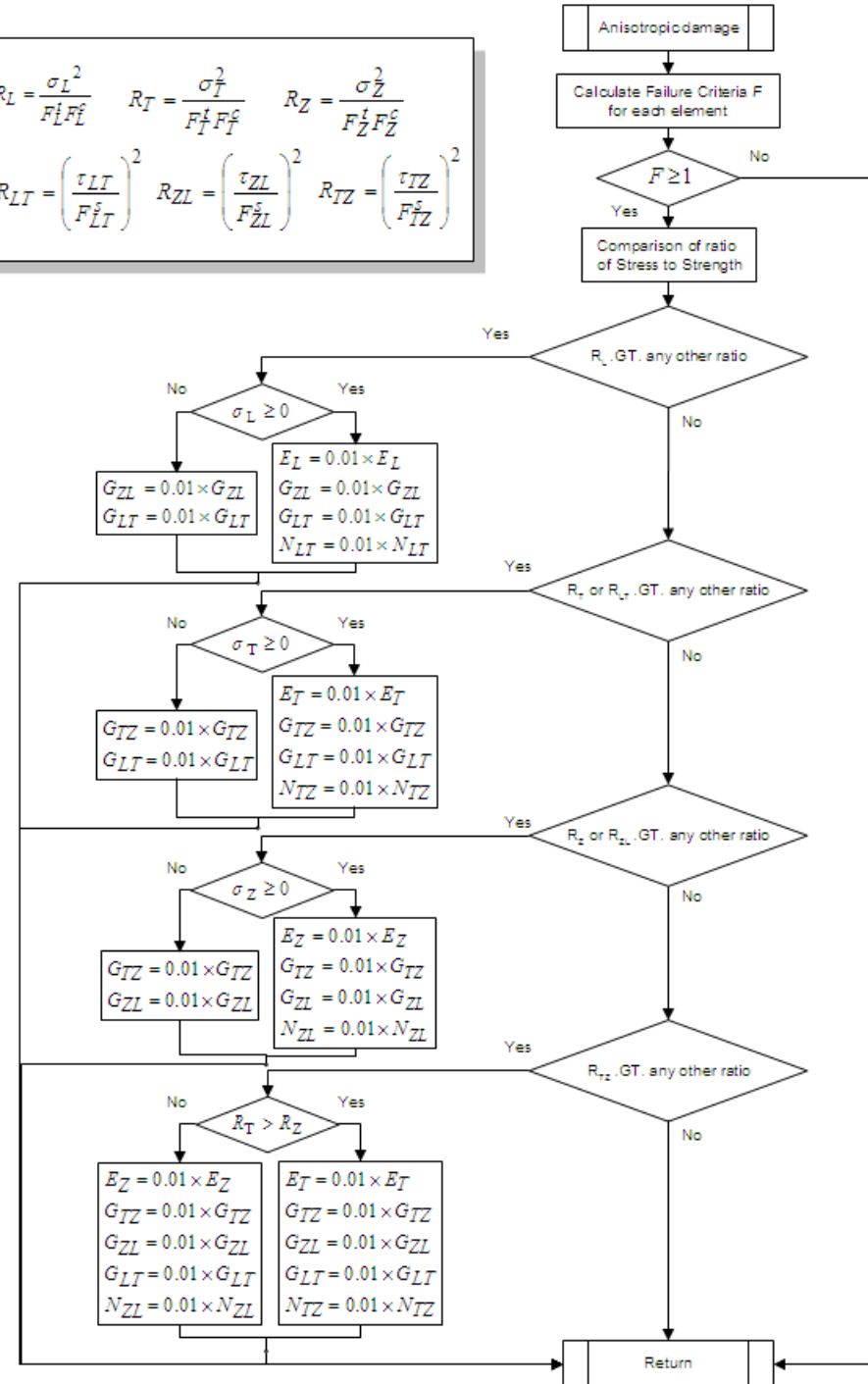
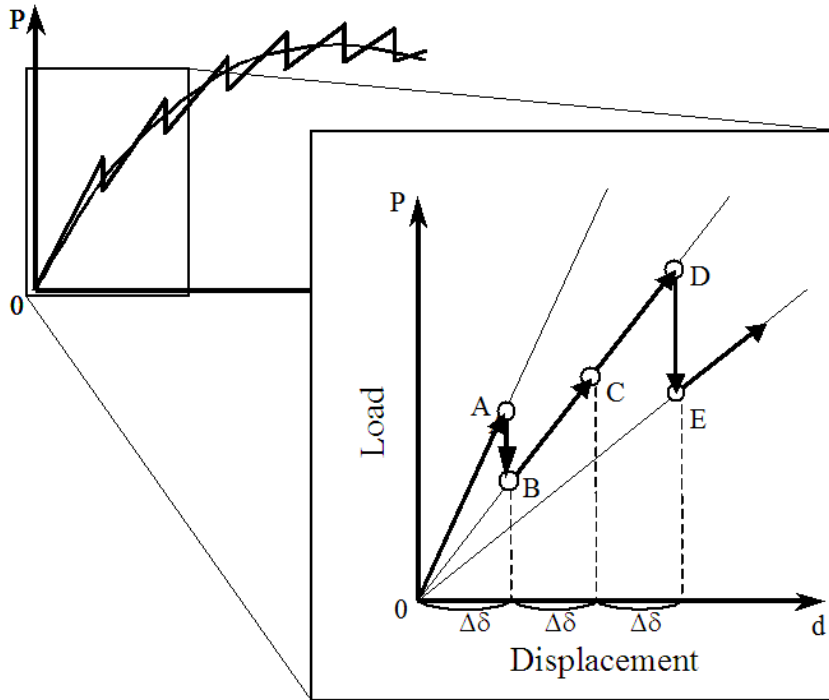
(d) Mode TZ

Maximum value	Damage Mode
$\frac{\sigma_i^2}{F_i^t F_i^c}$	Mode L
$\frac{\sigma_T^2}{F_T^t F_T^c}$ or $\left( \frac{\tau_{LT}}{F_{LT}^s} \right)^2$	Mode T&LT
$\frac{\sigma_Z^2}{F_Z^t F_Z^c}$ or $\left( \frac{\tau_{ZL}}{F_{ZL}^s} \right)^2$	Mode Z&ZL
$\left( \frac{\tau_{TZ}}{F_{TZ}^s} \right)^2$	Mode TZ

# Damage model (built-in in SACOM) – 2

$$R_L = \frac{\sigma_L^2}{F_L^i F_L^e} \quad R_T = \frac{\sigma_T^2}{F_T^i F_T^e} \quad R_Z = \frac{\sigma_Z^2}{F_Z^i F_Z^e}$$

$$R_{LT} = \left( \frac{\tau_{LT}}{F_{LT}^e} \right)^2 \quad R_{ZL} = \left( \frac{\tau_{ZL}}{F_{ZL}^e} \right)^2 \quad R_{TZ} = \left( \frac{\tau_{TZ}}{F_{TZ}^e} \right)^2$$



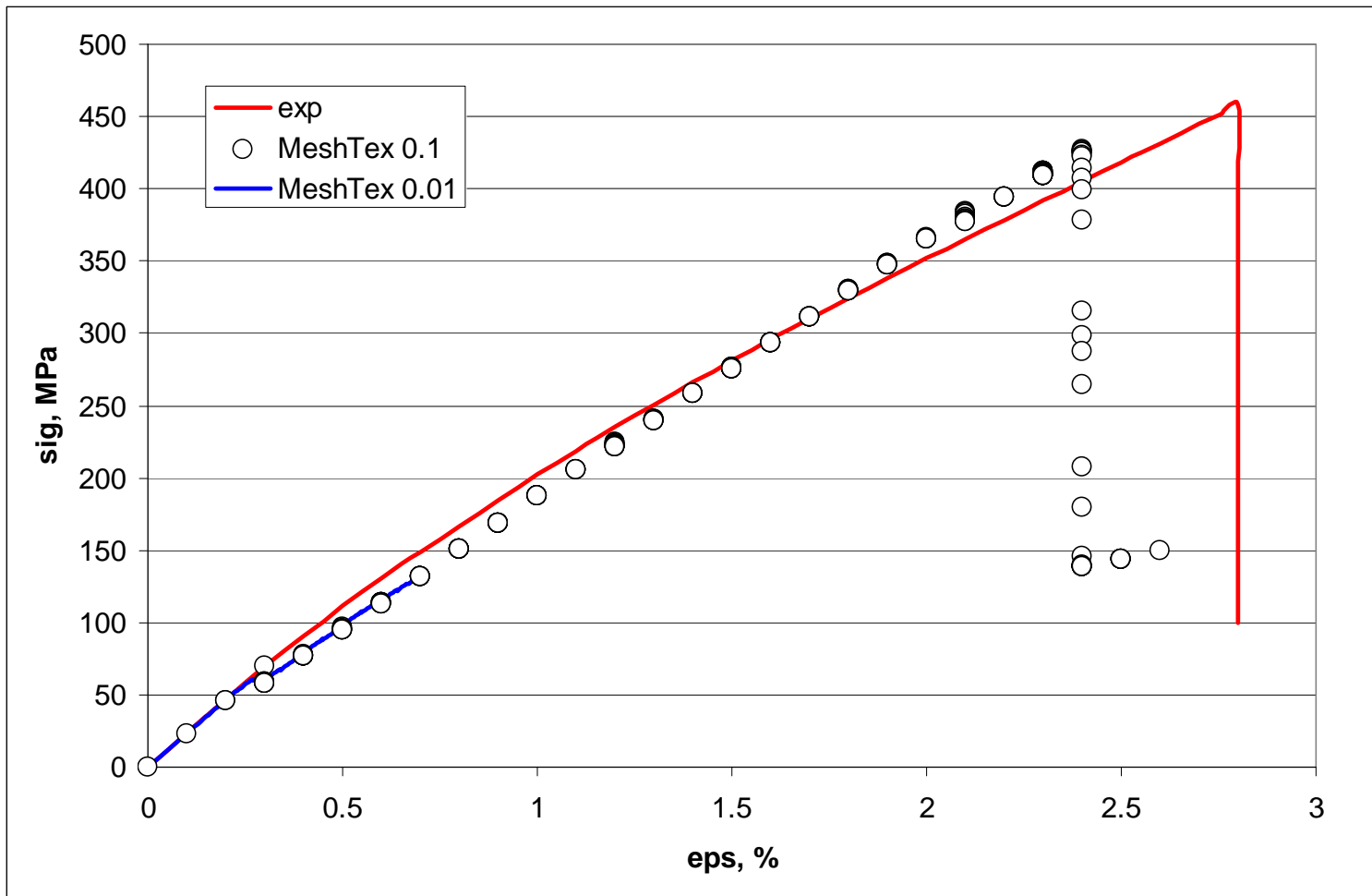


## Strength input data

UD	[1], VF=60%	[6], VF=55%	Hybon' data	<b>Corrected (L) for 75% and accepted for calculations</b>
L, tensile	1020	1080	1380	<b>1725</b>
L, compression	620	620		<b>620</b>
T, tensile	40	39		<b>40</b>
T, compr	140	128		<b>140</b>
LT	70	89		<b>70</b>
TZ				<b>70</b>
<b>Matrix</b>	tensile	76	Compression	112
	shear	88		

[1] "Composites Engineering Handbook" (P.K. Mallick, Ed.), Marcel Dekker, Inc., New York, 1997 (Table 1)

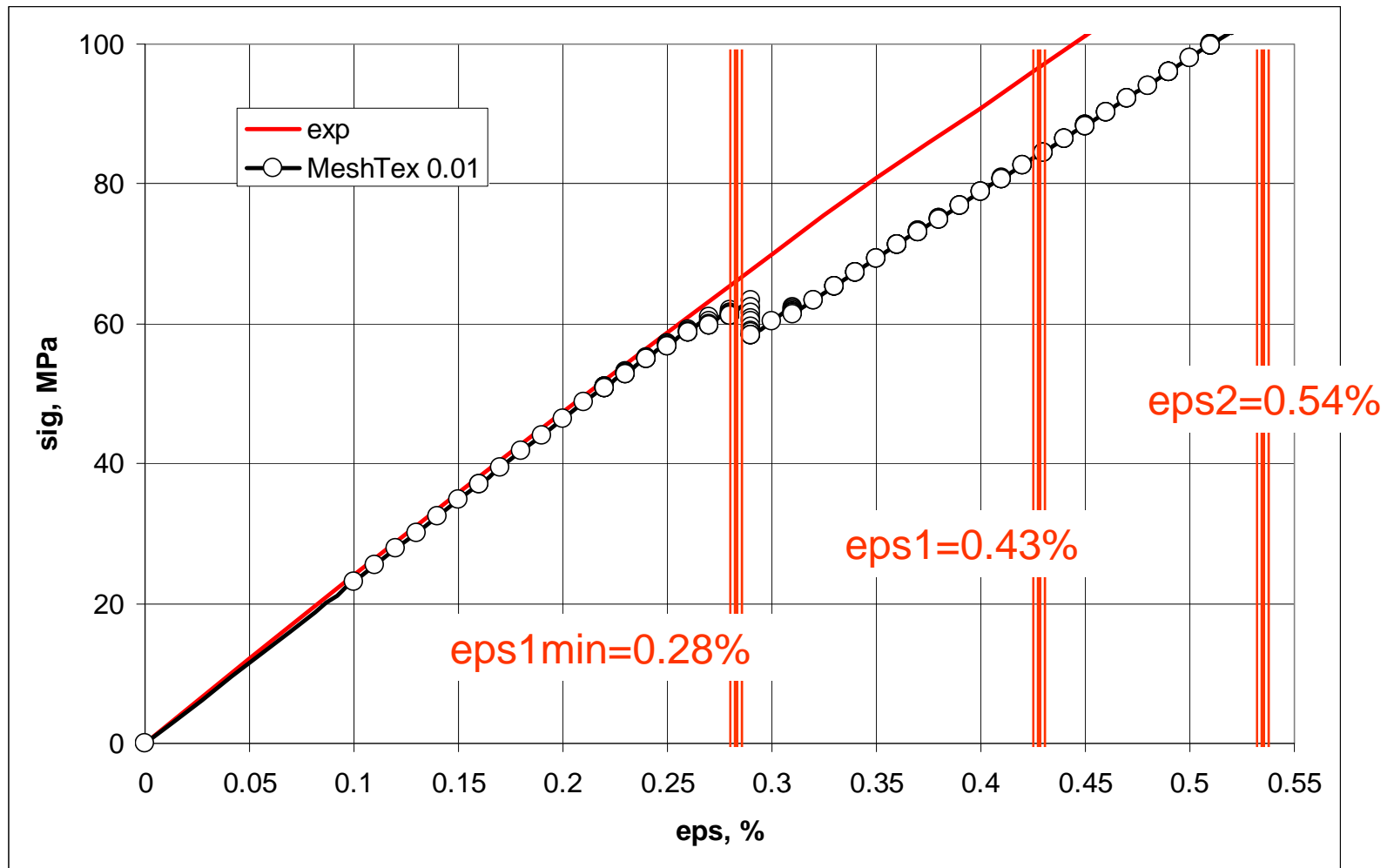
[2] "Engineering Mechanics of Composite Materials" by I.M. Daniel and O. Ishai, Oxford University Press, New York - Oxford, 1994 (Table 2.6),



correct change of stiffness

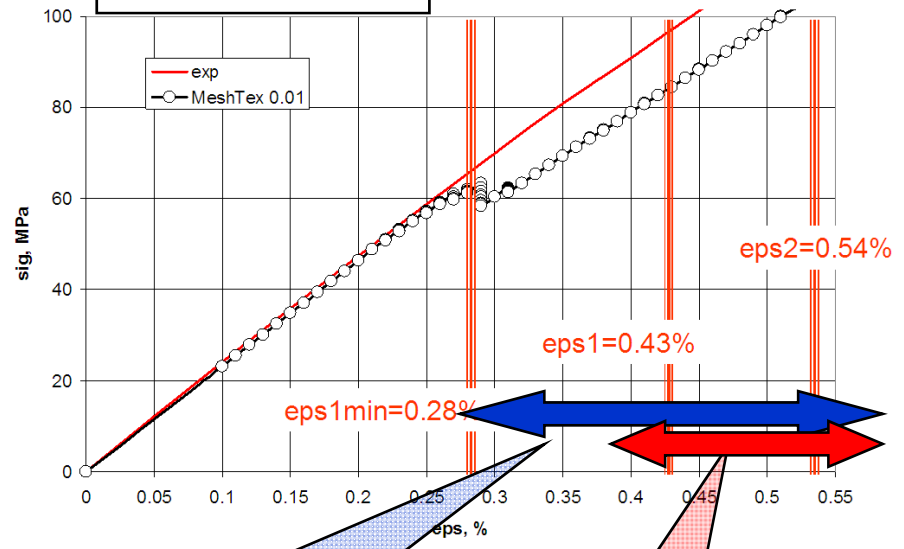
strength prediction depends on the assumed L-strength for UD

# Tensile diagram: Initial stage (step 0.01%)



# Predictions of the damage onset

## Experiment



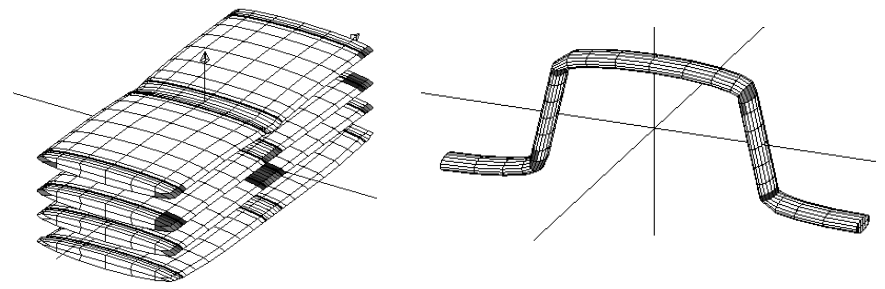
bundle-boundary cracks in Z-yarns

transverse cracks in fill

## FE, strain 0.22%

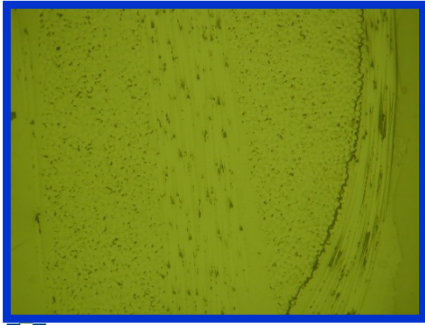
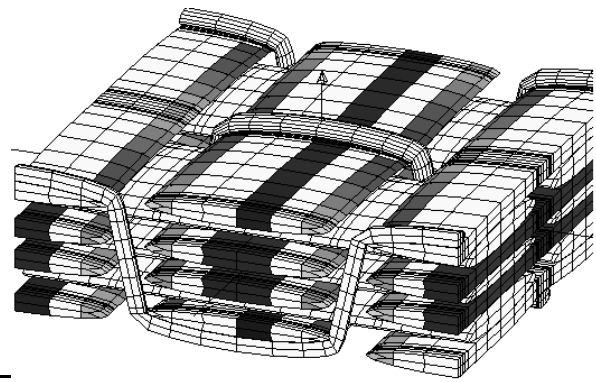
Damage starts at Z-yarn locations:

- T-mode at the edges of fill
- Z-mode in Z-yarns



## FE, strain 0.30%

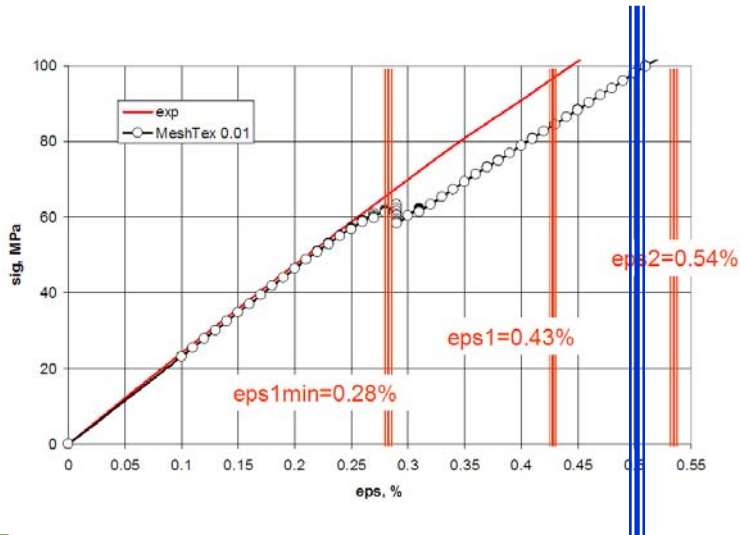
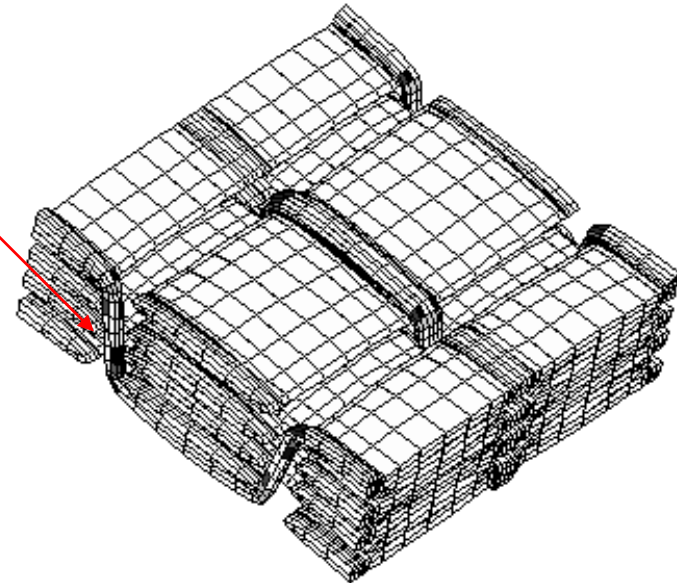
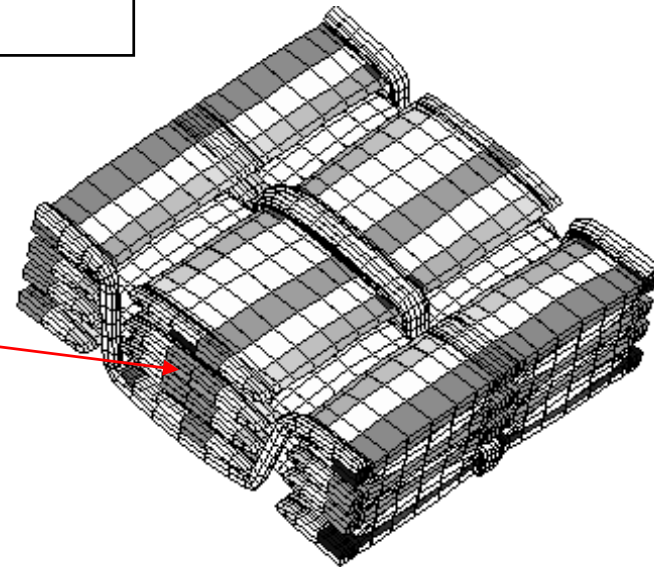
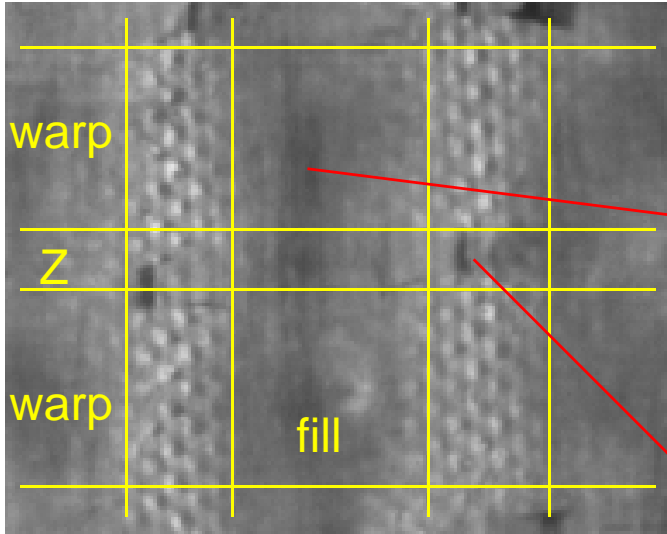
T-mode in fill



# Developed damage

Experiment: strain 0.5%

FE



1. Correct prediction of change of stiffness (tensile diagram)
2. Strength prediction directly depends on the assumed UD strength value
3. Estimation of the damage onset: within interval (eps1min, eps1)
4. Correct prediction of general character of the damage onset (location near Z-yarn)
5. No bundle-boundary damage mode; interpreted as Z-mode or T-mode near the surface of the yarns
6. Estimation of the onset of transversal damage: calculated too early (0.3% instead of  $0.43 \pm 0.04\%$ ). Depends on the assumed strength value.
7. Correct prediction of the extent of fill damage
8. In reality all the unit cells are not damaged simultaneously

NB: better results for the plain weave laminate, as the prevailing damage mode for it is transversal cracking



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<i>Fibres/matrix</i>	<i>Reinforcement</i>	<i>Publication</i>
	Experimental methodology in general	Comp Sci Tech <b>68</b> : 2340 (2008)
carbon/epoxy	NCF 0/90, $\pm 45$ , 0/-45/90/45	Comp A <b>36</b> : 1207 (2005)
	NCF $\pm 45$ , sheared	Comp A <b>39</b> : 1380 (2008)
	NCF 0/90, $\pm 45$ , toughened resin	SAMPE-Europe (2007)
	NCF tufted with carbon yarn*	Master thesis K.U. Leuven (2008)
	3-axial braid	Comp Sci Tech, in print
	Uniaxial braid*	Comp Sci Tech <b>68</b> : 2340 (2008)
	Uniaxial weave tufted with carbon*	ECCM-13 (2008)
	Woven twill 2/2	to be submitted to ICCM-17
glass/epoxy	Plain weave**	SAMPE-Europe (2008)
	3D woven (patented weaving process 3Tex)**	to be submitted to Comp A

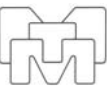
collaborations:

\* ITOOL consortium (EADS Innovation Works, Dassault Aviation, IFB – Stuttgart University)

\*\* 3Tex – A.E. Bogdanovich, D. Mungalov

Some of the experimental data will be made available in **Textile Composite Archive**:

[www.textilecomposite.tamu.edu](http://www.textilecomposite.tamu.edu)



<https://textilecomposite.tamu.edu/>

## Textile Composite Archive

This archive contains contributions from researchers around the world. The goal is to provide improved exchange of data and insights related to textile composites. This page provides links to web pages and data files that are maintained by each researcher. This is a work in progress.

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